

# RIVERTON CITY STORM DRAINAGE MASTER PLAN

AMENDMENT

(WEST OF BANGERTER HIGHWAY)

FINAL REPORT

June, 2004

# **RIVERTON CITY**

# STORM DRAINAGE MASTER PLAN

# WEST OF BANGERTER HIGHWAY

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#### **EXECUTIVE SUMMARY**

#### **INTRODUCTION**

This amendment to the storm drainage master plan is primarily for the portion of Riverton City west of Bangerter Highway. It also presents activities and public policies to effectively manage and regulate storm water runoff caused by development to mitigate flooding and environmental impacts throughout the City. The document will be a means for educating developers, private property owners, City staff and elected officials regarding the capability and needs of Riverton City's storm drainage system. The storm drainage study includes an examination of the existing storm drainage deficiencies are identified and the preferred solution alternatives to the deficiencies are presented with cost estimates.

A computer model was developed as part of the storm drainage master plan that simulates water runoff during a storm event in Riverton City. The storm drainage model operates within ArcView GIS and uses the HEC-1 Army Corps of Engineers Flood Hydrograph Package for computing the storm runoff hydrographs. Not only was the model a vital tool in analyzing the existing and future storm drainage situation for the master plan, but will allow Riverton City to continue to update and analyze for potential drainage deficiencies. This includes facilitating the analysis of conceptual design of alternative mitigation measures due to the impacts of new development.

### EXISTING STORM DRAINAGE SYSTEM EVALUATION

The area of Riverton City west of Bangerter Highway is new to development. Ten years ago development was essentially nonexistent and the land was used primarily for agricultural purposes. The only storm drainage features were open ditches along the roads, irrigation ditches and canals, and the natural washes and creeks flowing to the Jordan River. Major topographic relief for Riverton City is from the mountains on the west and south toward the Jordan River in the east. The storm drainage runoff in the study area eventually flows into Midas Creek to the North, Rose Creek to the south, the Provo Reservoir Canal that flows north through the middle of the study area, or past Bangerter Highway to the east through culverts.

Recent residential developments in the study area have been constructed with storm drainage pipes and retention/detention ponds to control storm runoff within the individual developments. The newer storm drainage facilities consist of properly graded lots to drain runoff away from homes and other buildings, streets and gutters to collect runoff, and storm drainage piping to convey the runoff to retention/detention basins.

Riverton City is fortunate to have Midas Creek and Rose Creek which flow through the City providing a convenient discharge location for the City's storm drainage facilities. Existing storm drainage facilities in Riverton City rely on these two creeks for the conveyance of storm water runoff to the Jordan River reducing the need for large main storm drain lines. Each creek system is under

the jurisdiction of Salt Lake County Department of Public Works. The 2002 Salt Lake County Southwest Creek and Canal Study provides guidance for creek channel improvements that correct years of disruptions by irrigation and farming activities. The general plan is for the Midas Creek and Rose Creek to be able to convey the historical or pre-development 100-year storm event (which produces about a 0.2 cfs per acre runoff rate) under future development conditions.

Butterfield Creek is a third natural creek located between Rose Creek and Midas Creek. Unfortunately, Butterfield Creek has become a problem the City of Riverton has had to address rather than a solution. Over 100 years ago, canals were constructed to flow from the south to the north perpendicular to the natural creeks. Flow from Butterfield Creek was intercepted by these canals and no longer reaches the lower portions of the valley. In addition, earlier development in Riverton City built in the path of Butterfield Creek because the channel was no longer contiguous. As new development has replaced farmland in the west portion of Riverton, runoff during storm events has increased beyond the capacity of the canals causing flooding. Restoring the natural channel for Butterfield Creek would be extremely costly and disruptive to existing development. Salt Lake County and Riverton City has decided not to restore or maintain Butterfield Creek. A major part of this study was to develop an alternative storm drainage route for areas tributary to Butterfield Creek in Riverton City.

The Provo Reservoir Canal, otherwise known as the Welby-Jacobs Canal, flows through the study area perpendicular to Rose Creek and Midas Creek. The canal is still used to deliver irrigation water, but also receives storm drainage. Canals are usually not the best conveyances for storm water because they are designed to distribute water rather than collect it. Canal capacities decrease from upstream to downstream, while runoff flowrates increase from upstream to downstream. Water quality, debris and sediment, liability issues, and canal maintenance are problems associated with use of the canals to convey storm drainage. Capacity and water quality issues have made the Welby-Jacobs Canal an unacceptable system to convey storm water.

Prior to this study, the only storm drain master plan for this area was a county-wide storm drain system. Riverton City has not previously included this area into the City storm drain master plan since it was annexed into the City in 1996. It became obvious that a comprehensive master plan was needed on August 21, 2001 when a storm produced a total of 1.49 inches of rain. With 1.1 inches of rain falling in 30 minutes, the rainfall event was classified as an 80-90 year storm by Salt Lake County. Prior to any development, a storm of this magnitude produced less runoff and mainly affected farmland. Even though the storm drainage systems within the new developments in the study area appear to be adequate, an outlet system or storm drainage system downstream of these developments does not exist.

Residential developments are being built in the City of Herriman just to the west of Riverton. The increased impervious area created by the new development is creating greater runoff tributary to Riverton City. During the August 21, 2001 storm, runoff from Herriman flooded homes and developments in Riverton City. Runoff then entered the Provo Reservoir Canal causing the canal to overtop the banks and flood homes on the eastside of the canal. This study will address these issues and others in providing solutions within the context of the master plan to minimize flooding.

# **MASTER PLAN PROJECTS**

The overall goal of the master plan projects is to convey storm runoff to Midas Creek or Rose Creek away from Butterfield Creek and the Provo Reservoir Canal. Flow historically tributary to Butterfield Creek will need to be conveyed to Midas Creek and Rose Creek. Commercial developments are required to have an on-site detention facility to detain runoff from a 100-year storm event and release at a rate of 0.2 cfs per acre. Storm runoff from residential developments is required to be detained in regional or local detention facilities (see Figure I). Residential developments not located within an area of a regional detention facility are required to have an on-site detention facility to detain runoff from a 100-year storm event and release at a rate of 0.2 cfs per acre. The duration of the 100-year storm event used to size a detention facility should be the duration that produces the largest volume of runoff in the detention facility given the allowable release rate. In addition, both commercial and residential development are to accommodate or identify a safe route for a storm event larger than a 100-year storm event.

Regional detention facilities are required to detain runoff from a 100-year storm event and release at a rate of 0.2 cfs per acre – with the exception of two areas. The first exception area is roughly between 13000 South and 13400 South and between 4300 West and 5000 West (see Figure I). This area is required to detain runoff from a 100-year storm event and release at a rate of 0.1 cfs per acre. Western Springs is the second exception area. It is located between 12600 South and 13000 South and 4570 West and 5000 West (see Figure I). This area is required to detain runoff from a 100-year storm event and release at a maximum flow rate of 5 cfs. These two exception areas require larger detention facilities and smaller release rates to compensate for conveying historical storm runoff from Butterfield Creek to Midas Creek and Rose Creek. Flow rates from any storm up to a 100-year event cannot be higher than the historical peak flow rates reported in the 2002 Salt Lake County Southwest Creek and Canal Study. The duration of the 100-year storm event used to size the detention facility should be the duration that produces the largest volume of runoff in the detention facility given the required release rate. In addition to accommodate or identify a safe route for a storm event larger than a 100-year storm event.

A master plan computer model was completed to help develop and analyze master plan projects (see Figure II). The master plan model analyzed the performance of the projects in future build-out conditions.

The master plan projects are listed in Table ES-1. The location of each project is shown on Figure III by project "ID Number". The flows and pipe diameters given in Table ES-1 are approximate and are for planning purposes only. A detailed hydraulic analysis should be performed during the design process for the master plan improvement projects to identify final design pipe sizes.





# KEY

- 24 Detention
- 23 Subbasin
- 22
- Subbasin Restricted to 0.2 cfs per acre in the model
  - 5 cfs Flow Restriction



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- 0.1 cfs per acre Flow Restriction
- Regional Detention Areas
- Study Boundary





#### RIVERTON CITY STORM DRAINAGE MASTER PLAN WEST OF BANGERTER HIGHWAY

# REGIONAL DETENTION AREAS AND DISCHARGE RESTRICTIONS

FIGURE I





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ESS A



# TABLE ES-1STORM DRAINAGE MASTER PLAN PROJECTS

ID	DESCRIPTION <sup>1</sup>	ESTIMATED COST <sup>2</sup>
1	Modify the retention pond at about 4570 W and Goshute with an outlet structure. Also, install 4500 feet of 24 inch diameter pipe to convey 22 cfs from the retention pond north in 4570 W to 12600 S and east in 12600 S to 4000 W. Install 2350 feet of 30 inch diameter pipe to convey 27 cfs from 12600 S and 4000 W north in 4000 W to about Swensen Farms Dr.	\$937,000
2	Install 1,400 feet of 21 inch diameter pipe to convey 7 cfs from about 13600 S to Rose Creek and 13400 S to Rose Creek in 4600 S.	\$126,000
3	Install 1,550 feet of 42 inch diameter pipe to convey 135 cfs from about 4600 W to Master Plan Project ID 4 detention basin in about 13200 S.	\$286,000
4	Construct an 8 acre-ft detention basin at about 4400 W and 13200 S and install 2,500 feet of 30 inch diameter pipe to convey 20 cfs from the detention basin to Rose Creek.	\$734,000
5	Install 1,600 feet of 30 inch diameter pipe to convey 29 cfs from about 5100 W in 13400 S to Master Plan Project ID 14 detention basin.	\$202,000
6	Install 2,500 feet of 30 and 36 inch diameter pipe to convey 50-70 cfs from about 4800 W to 5200 W in about 13600 S.	\$359,000
7	Install 1,600 feet of 30 inch diameter pipe to convey 23 cfs in 4600 W from about 13000 S to 13200 S.	\$207,000
8	Install 2,000 feet of 18 and 24 inch diameter to convey 7-15 cfs from about 4000 W and 13200 S to Rose Creek.	\$110,000
9	Install 1400 feet of 27 and 30 inch diameter pipe and a 1.5 acre-ft detention basin at about 4000 W and 12300 S.	\$309,000
10	Install 3,150 feet of 42 and 48 inch diameter pipe from about 4000 W and 13000 S to Rose Creek at about 13500 S and 3900 W.	\$623,000
11	Install 3,500 feet of 30 and 36 inch diameter pipe to convey 42-50 cfs from 3900 W and 13650 S to 3600 W and Rose Creek.	\$531,000
12	Install 1,800 feet of 36 inch diameter pipe to convey 75 cfs from 4600 W to 4800 W at about 13200 S.	\$285,000

# TABLE ES-1 STORM DRAINAGE MASTER PLAN PROJECTS (Continued)

ID	DESCRIPTION <sup>1</sup>	ESTIMATED COST <sup>2</sup>
13	Install 1,150 feet of 21inch diameter pipe to convey 4-7 cfs from about 11800 S South to Midas Creek in 4000 W.	\$104,000
14	Construct a 5 acre-ft detention basin at about 4800 W and 13600 S.	\$410,000
15	Install 1,000 feet of 18 and 24 inch diameter pipe and a 1 acre-ft detention basin at about 4130 W and 11900 S to Midas Creek.	\$160,000
16	Construct a waste way at Midas Creek and the Provo Reservoir Canal.	\$14,000
17	Install 1,200 feet of 21 inch diameter to convey 10 cfs from 13400 S and 4500 W to Rose Creek	\$108,000
18	Install 1,000 feet of 18 inch diameter pipe to convey 10 cfs from 4000 W and 12700 S to 12600 S and Bangerter Highway	\$83,000
19	Install 3,000 feet of 18 and 30 inch diameter pipe to convey 7-34 cfs from 4400 W to 3950 W at about 13000 S.	\$322,000
20	Install 1,000 feet of 18 inch diameter pipe to convey 4 cfs from 12800 S to 13000 S in 4400 W.	\$83,000
21	Install 1,300 feet of 18 inch diameter pipe to convey 9 cfs from about 4300 W and 12800 S to 4200 W and 13000 S.	\$108,000
22	Install 1,600 feet of 18 inch diameter pipe to convey 5 cfs in 4100 W from 12700 S to 13000 S.	\$133,000
23	Install 700 feet of 21 inch diameter pipe to convey 9 cfs at about 3950 W from 12800 S to 13000 S.	\$63,000
24	Install 1,000 feet of 36 inch diameter pipe in 4300 W from 12350 S to 12200 S.	\$158,000
25	Construct a waste way at Rose Creek and the Provo Reservoir Canal.	\$14,000
	TOTAL	\$6,474,000

1) The flows and pipe diameters given are approximate and are for planning purposes only. A detailed hydraulic analysis should be performed during the design process for the master plan improvement projects to identify final design pipe sizes.

2) Estimated construction costs include manholes, inlets, contingency, and engineering. Costs are in 2004 dollars.

## **FUNDING SOURCE OPTIONS**

Riverton City has the option to expand its authority as a Utah Municipal Corporation to establish a Storm Water Utility. Under this authority, the City can establish funding mechanisms necessary to support planned storm water system improvements as well as the day to day operations and maintenance of the existing system. The funding options available are similar to those established for other municipal utility functions. The flexibility established in Utah Code for sanitary sewers (and therefore for storm sewers) allows the City access to most generally accepted methods of public infrastructure financing. These funding options could include general obligation bonds, revenue bonds, State/Federal grants and loans, impact fees, and storm water management service charges (a Storm Water Utility). In reality, the City may need to consider a combination of these funding options.

# STORM DRAINAGE ORDINANCE AND DESIGN STANDARDS

Responsibilities regarding the Storm Drainage Plan should be incorporated into City design standards and/or ordinances. The City has the responsibility of implementing the Storm Drainage Master Plan. However, developers must also assume responsibility for conforming to the requirements of the Storm Water Master Plan. It is the developer's responsibility to comply with runoff restrictions, to show that the storm runoff which is generated upstream from the development can be conveyed through the development, and to demonstrate that runoff generated by the proposed development will not increase the impact of drainage waters on downstream property owners.

It is important that existing and future developments comply with runoff restrictions. Existing and future storm drain facilities were evaluated in the storm drain model assuming the allowable runoff restrictions will be achieved with detention facilities. If detention facilities are not constructed or properly maintained, runoff flowrates will exceed the capacity of the existing or future facilities. It is recommended that the City continue the design review and inspection practices that will ensure that runoff restrictions are met.

# RECOMMENDATIONS

- 1. The City should proceed with following the recommendations made in this report and construct the storm drainage master plan projects as the area of Riverton City west of Bangerter Highway develops. The City should also follow the recommendations made in the 2002 Salt Lake County Southwest Creek and Canal Study.
- 2. Model data should be updated as land use, conveyance, capacity, and detention are modified or constructed.
- 3. Commercial developments shall be required to detain their own runoff. Residential developments shall be required to detain their own runoff or be required to detain the runoff in a regional detention facility as appropriate for the location (see Figure I).

- 4. Regional and local detention facilities shall be designed to detain storm runoff from a 100year event and released at 0.1 cfs per acre, 0.2 cfs per acre, or 5 cfs as appropriate for the location (see Figure I). The duration of the 100-year storm event used to size the detention facility shall be the duration that produces the largest volume of runoff in the detention facility given the required release rate. All storm drain outfalls to Midas Creek or Rose Creek shall be approved by Salt Lake County Flood Control.
- 5. The City should consider adopting the site development storm drainage and erosion control plan submittal requirements included in Appendix D.

#### **CHAPTER I**

#### **INTRODUCTION**

This chapter provides an overview of the Riverton City Storm Drainage Master Plan project for west of Bangerter Highway. The following topics are presented in this section:

- Background
- Authority
- Study Activities
- Study Area
- Definitions

#### BACKGROUND

Riverton City is located in the southwest portion of the Salt Lake Valley. Developers have discovered Riverton City's large amount of undeveloped property in an attractive location. Riverton offers the feel of living in the country yet is located conveniently to an abundance of employment available in both Salt Lake County and Utah County. Riverton City is seeing a large increase in population. The area of the City experiencing a rapid rate of development is the portion of Riverton City west of Bangerter Highway.

Riverton City has decided to complete a storm drainage master plan in phases to be able to focus on key issues related to the rapid growth in the west portion of the City. This is allowing the City to spend their storm drain master plan budget more conservatively by addressing the pressing storm drainage issues first instead of completing a comprehensive master plan for the entire city. This report includes a study of the area in Riverton City west of Bangerter Highway.

Storm water runoff is a difficult resource to manage. In a dry climate such as Utah's, existing drainage ways are often dry and to the inexperienced citizen may appear to be prime places to construct buildings. Unlike sanitary sewers and culinary water systems, there are no clearly defined minimum service requirements for storm water systems. Storm water flows are dependent on many complex time and spatially varied factors. Even a natural undeveloped drainage system is not static: streams can erode in one section while depositing in another; stream courses can also change alignment and cross section dramatically with just one storm runoff event. Urbanization compounds the problem and creates a need for a drainage system with the basic goals of managing nuisance water, protecting development from damage, and protecting downstream waters from adverse quality and quantity impacts.

This storm drainage master plan for the portion of Riverton City west of Bangerter Highway presents activities and public policies to effectively manage and regulate storm water runoff caused by development to mitigate flooding and environmental impacts. The document will be a means for educating developers, private property owners, City staff and elected officials regarding the

capability and needs of Riverton City's storm drainage system. The storm drainage study includes an examination of the existing storm drainage system and future development impact on the system. Existing and future deficiencies are identified and the preferred solution alternatives to the deficiencies are presented with cost estimates. An implementation plan is developed with master plan projects.

A computer model was developed as part of the storm drainage master plan that simulates water runoff during a storm event in Riverton City. The storm drainage model operates within ArcView GIS and uses the HEC-1 Army Corps of Engineers Flood Hydrograph Package for computing the storm runoff hydrographs. Not only was the model a vital tool in analyzing the existing and future storm drainage situation for the master plan, but will allow Riverton City to continue to update and analyze for potential drainage deficiencies and facilitate the analysis of conceptual design of alternative mitigation measures.

#### AUTHORITY

Riverton City selected Hansen, Allen & Luce, Inc. (HAL) to assist them in preparation of a Storm Drainage Master Plan for the area west of Bangerter Highway. This study has been completed in accordance with an agreement between the Riverton City and HAL dated April 2001.

# **STUDY ACTIVITIES**

Specific tasks performed for this storm drainage study included:

## Task 1 - Review of Existing Master Plans and Facilities Inventory

Information contained in available reports and standards was reviewed and summarized to make use of these prior studies in this master planning process. Study activities for this task included the following:

- 1. Met with City Staff to review project objectives and obtain available drainage studies and standards.
- 2. Used available storm drainage facilities mapping, available "as builts", contour mapping and other additional information to prepare the existing facilities mapping in ArcView GIS.

#### Task 2 - Computer Model Development

A storm drainage computer model for the storm drainage and flood control system was prepared to evaluate the performance of the existing facilities and to confirm the effect of recommended improvements. The City was provided an in house computer model which can be used by City staff on a day to day basis to meet City needs. The model works directly with the City's Geographical Information System. Study activities for this task included the following:

- 1. Assisted the City in selection of the storm drainage model. Reviewed the advantages and disadvantages of available storm drainage models.
- 2. Drainage basin, subbasin boundaries, and flow paths were delineated using aerial photography mapping, contour data, and drainage basin maps from previous studies.
- 3. Met with City staff to review drainage basin boundaries and existing hydrologic characteristics. Subbasin boundaries were modified based on input from the City.
- 4. Using the facilities inventory coverage (Task 2 above), a model of the storm drainage conveyance system was prepared and the existing capacity of the conveyance system facilities were assessed.
- 5. Using available mapping, field reconnaissance, and land use planning, hydrologic characteristics for each subbasin were developed for existing conditions.
- 6. Using land use planning, subbasin hydrologic characteristics for the future planning period were predicted.
- 7. Input data files were prepared to run the storm drainage model.
- 8. Runoff hydrographs at key locations for the existing storm drainage facilities were computed. Critical storm durations were found by performing a duration sensitivity analysis using the 1, 3, and 6-hour storm durations. The storm drainage model was calibrated qualitatively through evaluation with City personnel.
- 9. Runoff outflow hydrographs for each subbasin under future conditions were computed.
- 10. A manual of the GIS computer model was prepared.

# Task 3 - Existing System Evaluation

The existing storm drainage facilities were evaluated and deficiencies were identified in regards to the storm drain network, detention basin storage, and other difficulties encountered during the investigation. Study activities for this task included the following:

- 1. Evaluated adequacy of existing facilities to meet existing and future needs. Defined areas of deficiency such as lack of storm drain capacity, inadequate detention volume, inadequate natural channel capacity, and erosion and maintenance problems.
- 2. Located existing and future problem areas on GIS coverage.

# Task 4 - Recommendations

A master storm drainage plan was prepared, including recommendations for immediate and future improvements. Study activities for this task included the following:

- 1. Evaluated, with City staff, potential locations for storm water detention facilities.
- 2. Met with City personnel to develop and screen conceptual level drainage plans with alternatives that included detention, flood channels, storm drains, etc.
- 3. Compared the alternative plans on the basis of conceptual level construction costs, maintenance requirements, public acceptability, and ability to accommodate changes in the City's land use plan.

- 4. Met with City personnel to evaluate the drainage plan alternatives to help the City select the preferred alternative.
- 5. Refined the preferred drainage plan and prioritized recommendations into immediate and future improvement recommendations. (Future was defined as build-out development).
- 6. Developed a draft of the Capital Improvement Plan for the portion of the City west of Bangerter Highway, including estimated construction costs for the improvements.

# Task 5 - Master Plan Document Preparation

A report was prepared, documenting the capability and needs of the Riverton City storm drainage system west of Bangerter Highway. The document will be a means for educating developers, private property owners, City staff and elected officials regarding the capability and needs of Riverton City's storm drainage system. Study activities for this task included the following:

- 1. Prepared a draft table of contents and outline. Met with City staff to review the draft outline, receive suggestions, and revise the outline as needed to meet City needs.
- 2. Prepared Draft Master Plan Document.
- 3. Presented the draft document to City staff for review.
- 4. Received comments and prepared the Final Master Plan Document.

# **STUDY AREA**

The study area included all of the area within Riverton City boundaries west of the Bangerter Highway (See Figure I).

# **DEFINITIONS**

Initial storm drainage system:	The drainage system which provides for conveyance of the storm runoff from minor storm events. The initial drainage system usually consists of curb and gutter, storm drains, and local detention facilities. The initial drainage system should be designed to reduce street maintenance, control nuisance flooding, help create an orderly urban system, and provide convenience to urban residents.
Major storm drainage system:	The drainage system that provides protection from flooding of homes during a major storm event. The major storm drainage system may include streets (including overtopping the curb onto the lawn area), large conduits, open channels, and regional detention facilities
Minor storm event:	Storm event which is less than or equal to a 10-year storm.

Major storm event:	Generally accepted as the 100-year storm.
10-year storm:	The storm event that has a 10-percent (1 in 10) chance of being equaled or exceeded in any given year.
100-year storm:	The storm event that has a 1-percent (1 in 100) chance of being equaled or exceeded in any given year.
500-year storm:	The storm event that has a 0.2-percent (1 in 500) chance of being equaled or exceeded in any given year.
Cross drainage structures:	Structures that convey storm drainage flows from one side of the street to the other and normally consist of storm drains or culverts.
Retention basin:	An impoundment structure designed to contain all of the runoff from a design storm event. Retention basins usually contain the runoff until it evaporates or infiltrates into the ground.
Detention basin:	An impoundment structure designed to reduce peak runoff flowrates by detaining a portion of the runoff during periods of peak flow and then releasing the runoff at lower flowrates.
Storm frequency:	A measure of the relative risk that the precipitation depth for a particular design storm will be equaled or exceeded in any given year. This risk is usually expressed in years. For example, a storm with a 100-year frequency will have a 1-percent chance of being equaled or exceeded in a given year.
Storm duration:	The length of time of a storm event, from the beginning of rainfall to the point where no further accumulation of precipitation is occurring.
Storm intensity:	The rate at which precipitation accumulates during a storm event.
Storm depth:	The total depth of precipitation produced by a storm event.
Design rainstorm:	A rainfall event, defined by storm frequency, storm duration, and rainfall distribution, that is used to design drainage structures or conveyance systems.
HEC-1:	The Flood Hydrograph Package developed by the U.S. Army Corps of Engineers used to model storm runoff.

#### **CHAPTER II**

#### **EXISTING STORM DRAINAGE SYSTEM EVALUATION**

This chapter includes an overview of the Riverton City storm drainage system west of Bangerter Highway followed by an assessment of the adequacy of the system.

## **OVERVIEW OF EXISTING SYSTEM**

The area of Riverton City west of Bangerter Highway is new to development. Ten years ago development was essentially nonexistent and the land was used primarily for agricultural purposes. The only storm drainage features were open ditches along the roads, irrigation ditches and canals, and the natural washes and creeks flowing to the Jordan River. Major topographic relief for Riverton City is from the mountains on the west and south toward the Jordan River in the east. The storm drainage runoff in the study area eventually flows into Midas Creek to the North, Rose Creek to the south, the Provo Reservoir Canal that flows north through the middle of the study area, or past Bangerter Highway to the east through culverts.

Recent residential developments in the study area have been constructed with storm drainage pipes and retention/detention ponds to control storm runoff from the individual developments. The newer storm drainage facilities consist of properly graded lots to drain runoff away from homes and other buildings, streets and gutters to collect runoff, and storm drainage piping to convey the runoff to detention basins.

Each aspect of the existing storm drainage system for the study area will be discussed in greater detail in the following paragraphs.

# **Creeks and Canals**

Riverton City is fortunate to have Midas Creek and Rose Creek which flow through the City providing a convenient discharge location for the City's storm drainage facilities. Existing storm drainage facilities in Riverton City rely on these two creeks for the conveyance of storm water runoff from the City to the Jordan River reducing the need for large main storm drain lines. Each stream system is under the responsibility of Salt Lake County Department of Public Works. The 2002 Salt Lake County Southwest Creek and Canal Study Midas Creek provides guidance for Midas Creek and Rose Creek channel improvements and future watershed developments. The general plan is for the creeks to be able to convey the pre-development 100-year storm event under future development conditions.

Butterfield Creek, on the other hand, was abandoned as a county maintained drainage facility and is no longer under the responsibility of Salt Lake County Department of Public Works. In addition, Butterfield Creek is unable to convey runoff to the Jordan River because of modifications to the natural creek channel from over 100 years of farming, canal construction and development. Lastly, the Provo Reservoir Canal cannot effectively convey storm runoff. Each of the creeks and the canal in the study area are described individually in the following paragraphs.

#### **Midas Creek**

Midas Creek generally drains the northern portion of the City. It flows east, from the mountains on the west side of Riverton City, to the Jordan River. The 2002 Salt Lake County Southwest Creek and Canal Study outlines projects for Midas Creek that would provide capacity in the Creek to convey a 100-year storm event with historical runoff flow rates of 0.2 cfs per acre. The projects also provide capacity in Midas Creek for runoff historically tributary to Butterfield Creek west of 6000 West. Salt Lake County's goal is to provide capacity for the historical or predevelopment 100-year storm event.

#### **Rose Creek**

Rose Creek drains the southern portion of the City. It flows from the mountains southwest of Riverton City west to the Jordan River. Similar to Midas Creek, the Rose Creek channel has been disrupted by irrigation and farming activities. Rose Creek drainage area has also had a history of large amounts of sediment deposition. The 2002 Salt Lake County Southwest Creek and Canal Study outlines projects to allow Rose Creek to convey the pre-development 100-year storm event. A number of improvements have been completed. Salt Lake County's goal is to provide capacity for the pre-development 100-year storm event defined in the study.

#### **Butterfield Creek**

Butterfield Creek is a third natural creek located between Rose Creek and Midas Creek. Much of Butterfield Creek has unfortunately is no longer continuous. Over 100 years ago canals were constructed to flow from the south to the north perpendicular to the natural creeks. Flow from Butterfield Creek was intercepted by these canals and no longer reached the lower portions of the valley. Also, farming activities disrupted portions of the historical channel. Earlier development in Riverton City built in the path of Butterfield Creek because of an absence of the threat of flooding. As new development has replaced farmland in the west portion of Riverton, runoff during storm events has increased beyond the capacity of the canals which has caused flooding.

Restoring the natural channel for Butterfield Creek would be extremely costly and disruptive to existing development. Salt Lake County and Riverton City has decided not to restore or maintain Butterfield Creek. The 2002 Salt Lake County Southwest Creek and Canal Study indicates that the Butterfield Creek channel disappears at 6000 West. The study recommends that a new conduit be installed in 6000 West to convey all runoff from the end of Butterfield Creek at 6000 West to Midas Creek (page 7-7). A major part of this study was to develop a solution for Butterfield Creek drainage east of 6000 West in Riverton City.

#### **Provo Reservoir Canal**

The Provo Reservoir Canal, otherwise known as the Welby-Jacobs Canal, flows through the study area perpendicular to Rose Creek and Midas Creek. The canal is still used to deliver irrigation water and receives storm drainage. Canals are usually not the best conveyances for storm water because they are designed to distribute water rather than collect it. Canal capacities decrease from upstream to downstream, while runoff flowrates increase from upstream to downstream. Water quality, debris and sediment, liability issues, and canal maintenance are problems associated with use of the canals to convey storm drainage. The City and the canal owners would rather not have canals as the primary point of discharge. The city may need some metered releases into canals to address some storm water issues.

#### Detention

Detention basins have been built for new residential developments to minimize the impact of the development on storm drainage runoff. Also, various temporary detention/retention ponds have been necessary due to incomplete conveyance systems down stream. The County has required all runoff from development to be detained before entering Rose Creek or Midas Creek. As part of this study, the existing detention basins in the study area were analyzed.

# **Storm Drains And Ditches**

Capacities of storm drainage pipes were estimated based upon the pipe slope, pipe material type, and Manning's equation. Where pipe slope was not provided in the City facilities inventory, slope was assumed based on ground surface contours using 2-foot contour mapping. Estimated pipe capacities are based upon conceptual level engineering and do not consider limitations due to inlet capacities or downstream restrictions. Estimated capacities also do not consider allowable surcharging that might provide additional capacity. While the estimated capacities may not be precise, they are consistent with the precision of the runoff estimates and are sufficient for drainage planning efforts.

The capacity of the curb and gutter was estimated for a standard residential street with the water surface level with the top of the curb. Maximum flow capacities were calculated with Manning's equation for gutter slopes from 0.3 to 10 percent. Because gutters are usually obstructed by parked cars or other obstacles, the maximum flow capacity was reduced to an allowable capacity according to a methodology outlined in the *Urban Storm Drainage Criteria Manual* (Denver Regional Council of Governments, 1990). This methodology applies a reduction factor to the maximum capacity to estimate the allowable capacity of the gutter. The reduction factor is a function of the gutter slope. Curb and gutter capacity varies from 4 to 8 cfs for the typical range of slopes allowed on residential streets. Gutter capacity was not considered unless the model indicated peak runoff was exceeding the capacity of a pipe and the pipe was installed in a street with gutters.

Most of the ditches in the study area are roadside ditches along older roads. Based on discussions with City staff, roadside ditches are planned to be replaced with storm drain pipe when the older roads are improved. It was assumed in this study that all of these ditches will be replaced with piped storm drain systems for the future.

#### ADEQUACY OF EXISTING STORM DRAINAGE FACILITIES

Prior to this study, the only storm drain master plan for this area was a county-wide storm drain system. Riverton City has not previously included this area into the City storm drain master plan since it was annexed into the City in 1996. It became obvious that a comprehensive master plan was needed on August 21, 2001 when a storm produced a total of 1.49 inches of rain over a duration of 60 minutes. With an intensity of 1.1 inches of rain falling in 30 minutes, the rainfall event was classified as an 80-90 year storm by Salt Lake County. Prior to any development, a storm of this magnitude produced less runoff and mainly affected farmland. Even though the storm drainage systems within the new developments in the study area appear to be adequate, an outlet system or storm drainage system downstream of these developments does not exist.

Residential developments are being built in the City of Herriman just to the west of Riverton. The increased impervious area created by the new development is creating greater runoff tributary to Riverton City. During the August 21, 2001 storm, runoff flooded homes and uncompleted developments in Riverton City. Runoff then entered the Provo Reservoir Canal until the canal overtopped the banks and flooded homes on the eastside of the canal.

Both the models of existing and future conditions were used to evaluate the existing storm drainage system. Existing storm drainage deficiencies for the study area were identified using the storm drainage system models, as well as by Riverton City staff based upon field experience.

#### **CHAPTER III**

#### STORM DRAINAGE COMPUTER MODEL DEVELOPMENT

This chapter describes the methodology and process behind the storm drainage model for Riverton City. First, the hydrology and basin characteristics will be discussed followed by a model description.

## HYDROLOGY AND BASIN CHARACTERISTICS

#### **Drainage Design Frequency**

The approach selected by Riverton City for determining the drainage design frequency is based upon methodology given in the *Urban Storm Drainage Criteria Manual* (Denver Regional Council of Governments, 1990). The *Urban Storm Drainage Criteria Manual* defines the urban drainage system as follows:

"Every urban area has two separate and distinct drainage systems, whether or not they are actually planned for and designed. One is the initial system, and the other is the major system. To provide for an orderly urban growth, reduce costs to future generations, and obviate loss of life and major property damage, both systems must be planned and properly engineered."

The initial storm drainage system is sometimes referred to as the convenience system in that the initial system is designed to "reduce street maintenance costs, to provide protection against regularly recurring damage from storm runoff (of a 10-year recurrence interval or less), to help create an orderly urban system, and to provide convenience to the urban residents" (Denver Regional Council of Governments, 1990). Storm sewer systems are generally considered part of the initial storm drainage system. In conjunction with the initial storm drainage system, provisions should be made to avoid major property damage or loss of life from a major storm event. Such provisions are considered to comprise the major storm drainage system.

The major storm drainage system in newly developing urban areas or business districts should generally be designed for the 100-year event with the objective to eliminate major damage to edifices (homes, buildings, etc.) and to prevent loss of life. This does not mean that storm sewers (which are considered part of the initial storm drainage system) should be designed for the 100-year event. It means that the combination of storm sewers and channelized surface flow, which may include using part of the grassed frontage area of a home as part of a 100-year channel (see Figure IV), should be designed to accommodate the 100-year event thereby preventing damage to the edifice. There appears to be general agreement among most major flood control agencies that in the design of the major storm drainage system for urban areas the 1-percent storm (100-year return period) should be used, except in the design of water impoundment structures that exceed a specified capacity.





URBAN STORM DRAINAGE CRITERIA FIGURE IV Riverton City has selected the 10-year storm event for the design of the initial storm drainage system and the 100-year storm event for design of the major storm drainage system. The 10-year storm event was selected by Riverton City for the design of the initial storm drainage system because:

- 1. The 10-year storm event is the design frequency selected by most large municipalities along the Wasatch Front, and
- 2. The 10-year storm event provides a level of protection most likely experienced historically throughout much of Riverton City.

Applying the storm drainage criteria (100-year storm event) to the major storm drainage system in Riverton City is a more complex issue, because the major storm drainage system in Riverton City is very difficult to define and analyze. In most of the newer developments, roadways are lower in elevation than adjacent lots which allow the roadways to carry the runoff that exceeds the capacity of the initial storm drainage system. However, the older sections of Riverton City were developed around an existing open channel irrigation system where ditches along roadways deliver irrigation water to adjacent lots and agricultural land. The ditches along the roadways must be higher than the lots, so the roadways are higher in elevation than adjacent properties. Runoff that exceeds the capacity of the initial storm drainage system will collect in low areas between the homes and the roadways, and in some cases may flow through lots between homes. Determining the local storage in existing lots and identifying flow patterns for the 100-year storm event, is not feasible with the topography information that is currently available. Although the 100-year storm event was not analyzed as part of this study, it is recommended that Riverton City apply the major drainage system design criteria (100-year storm event) to new development whenever it is appropriate.

#### **Design Rainstorm**

The Rainfall Intensity Duration Analysis, Salt Lake County, Utah, (TRC North American Weather Consultants and Meteorological Solutions Incorporated, 1999), was used to develop design rainstorm depths for the study area. The TRC report gives design rainfall depths for storms with durations of 1- hour and 6-hours. Rainfall depth for the 3-hour design storm was determined using a linear regression equation.

The rainfall depths during a 10-year storm for the study area are: 0.88 inches for a 1-hour duration, 1.13 inches for a 3-hour duration, and 1.38 inches for a 6-hour duration. The rainfall depths during a 100-year storm for the study area are: 1.44 inches for a 1-hour duration, 1.65 inches for a 3-hour duration, and 1.85 inches for a 6-hour duration.

The storm duration that will produce the highest peak runoff flow rate is dependent on rainfall-duration relationships, the characteristics of the basin, and upon the level of detention storage. Generally speaking, the longer runoff takes to flow through a drainage basin or detention basin, the longer the critical storm duration. A duration sensitivity analysis of the hydrologic study area was performed by successive model runs using 1-hour, 3-hour, and 6-hour storm durations. The

6-hour storm duration was found to govern peak runoff flowrates downstream from detention basins. The 1-hour storm duration was usually found to produce the largest peak runoff flowrates for local areas upstream from detention basins.

To compute runoff from a given storm, the distribution of the rainfall through time must be known. Critical runoff events from urban areas along the Wasatch Front are caused by cloudburst type storms, characterized by short periods of high intensity rainfall. During the 1960's and early 1970's, Dr. Eugene E. Farmer and Dr. Joel E. Fletcher completed a major study of the precipitation characteristics for storms in northern Utah. This effort has become the definitive source for rainfall distributions appropriate for the Wasatch Front area. In Davis County, Farmer and Fletcher (1971) examined rainfall gage records and classified storms based on whether the heaviest rainfall of the storm fell in the first, second, third, or fourth quarter of the storm period. Farmer and Fletcher found that "first and second quartile storms together comprise 76 percent of those storms containing a burst of 5-minute duration, with a 2-year recurrence interval and 92 percent of storms containing a burst of 10-minute duration, with a 10-year recurrence interval." Farmer and Fletcher developed model storms for first and second quartile storms. The second quartile storm distribution produces the higher runoff peaks and is the rainfall distribution used in this study for runoff hydrograph calculations (see Figure V).

FIGURE V FARMER AND FLETCHER 2<sup>ND</sup> QUARTILE STORM DISTRIBUTION



# **Drainage Basin Characteristics**

A drainage basin is an area where all storm runoff within the area will collect to a common point. Another name for a drainage basin is watershed or catchment. Subbasins are smaller drainage basins located within a larger drainage basin. Drainage subbasin boundaries depend upon both the topography and the location of storm drainage facilities. The drainage subbasin boundaries delineated for the master plan model are shown on Figure II.

Subbasins characteristics were developed based on field observations and the GIS mapping supplied by Riverton City. Important subbasin characteristics included:

- Subbasin area / Topography
- Hydrologic soil type
- Percentage of impervious area
- SCS curve number
- Conveyance characteristics

Hydrologic characteristics of each subbasin are given in the model output provided in Appendix A. Subbasins with connectivity numbers are on Figure II.

# Subbasin Area

Subbasins were delineated within the GIS database using topographic mapping and the locations of storm drainage facilities. Digital base mapping of Riverton City consisted of 2-foot contours with physical features such as property lines, canals, and streets. Subbasins varied in size depending upon the level of development within the subbasin and the locations for which hydrographs were needed. Average subbasin size in developed areas was approximately 30-acres. Each mountain watershed, directly tributary to Riverton City, was delineated as a single subbasin.

# Hydrologic Soil Type

Hydrologic soil type is a general indication of the soil's infiltration capacity. Soils are assigned a hydrologic type of A, B, C, or D by the Natural Resource Conservation Service (NRCS). Soils of hydrologic soil type A have the highest infiltration rate, and therefore produce the least amount of runoff. Soils of hydrologic soil type D have the lowest infiltration rate, and therefore produce the highest amount of runoff. Most of soils within study area are hydrologic soil type C. Each subbasin was assigned a hydrologic soil type based upon the NRCS mapping.

#### **Impervious Area**

Impervious areas within each subbasins were estimated using the GIS model. The impervious area was divided into two components, directly connected impervious areas and unconnected impervious areas. Directly connected impervious areas provide a direct path for runoff from the impervious area to a conveyance such as a pipe, gutter, or channel. Directly connected impervious areas include roadways, parking lots, driveways, and sometimes the roofs of buildings. Runoff from unconnected impervious areas must cross a pervious area before reaching a conveyance. Examples of unconnected impervious areas include sidewalks that are not adjacent to the curb, patios, sheds, and usually some portion of the roof of a house.

It is important to distinguish between directly connected and unconnected impervious areas because runoff from the directly connected impervious areas reaches the drainage conveyance system quickly and usually determines the magnitude of the peak flow rate upstream from detention. Because of the permeable soils in the study area, unconnected impervious areas such as back yard patios which drain to grassed or landscaped areas have much less impact on storm runoff peak flows. Based upon field observations, the directly contributing impervious area for a typical residential lot in Riverton City is assumed to include the driveway, and 50 percent of the home and garage area. It is assumed that runoff from the remaining 50 percent of the home and garage area flows over grassed areas before reaching the street. For large commercial structures, it was assumed that 100 percent of the roof area is directly connected impervious area.

#### **SCS Curve Number**

Each basin was assigned an SCS curve number. The curve number describes the relationship between precipitation and runoff for the pervious and unconnected impervious portions of the subbasin. Curve numbers for each subbasin were estimated using a methodology presented by the Soil Conservation Service (SCS, 1972).

#### Future Land Use and Hydrologic Characteristics

Many large portions of Riverton City west of Bangerter Highway have not been fully developed. Current zoning and land use maps were used to determine the future land use for full buildout. Future hydrologic characteristics for the existing undeveloped subbasins were changed to reflect anticipated conditions when developed. Future percentage of impervious area for currently undeveloped subbasins was estimated based upon current zoning and land use in similar adjoining property that has already been developed.

# **MODEL DESCRIPTION**

The Riverton City Storm Drainage Model is a combination of an ArcView GIS model and the Army Corps of Engineers (COE) "Flood Hydrograph Package (HEC-1)" linked by the Hydrologic Model Interface (HMI). HMI is a custom user interface developed by HAL to operate within the ArcView GIS environment. HMI provides an interactive link between the user, the GIS database, and HEC-1. A description of the model is contained in Appendix B.

The Riverton City Storm Drainage Model incorporates the Army Corps of Engineer's "Flood Hydrograph Package (HEC-1)" for calculation of runoff hydrographs. HEC-1 can be used for both urban and rural watershed models. HEC-1 allows use of both the Soil Conservation Service (SCS) curve number and unit hydrograph method for modeling undeveloped watersheds, and the kinematic wave modeling method for urban areas. The HEC-1 input file is written by HMI from the information within the GIS database. Sources used to create the GIS database and calculate hydrological characteristics for the Riverton City Storm Drainage Model include:

- "Soil Survey, Utah County, Utah" (SCS, 1968).
- Aerial photo mapping and contour data from Salt Lake County.
- Digital mapping from Riverton City
- $7-\frac{1}{2}$  Minute U.S. Geological Survey topographical maps.
- Curve number selection procedures provided by the Soils Conservation Service (SCS, 1972).
- Field reconnaissance.

# **Model Components**

The Storm Drainage Model is comprised of five major components. Each of these model components is described below.

- **Subbasin Elements** Subbasins are the basic elements for which runoff hydrographs are calculated. Subbasin elements represent a geographic area, and they are described by all of the hydrologic characteristics required by HEC-1 for calculation of a runoff hydrograph. Subbasins are identified on Figure II. Hydrologic characteristics of the subbasin elements are discussed in previous sections.
- **Conveyance Elements** Conveyance elements are used to represent routing of runoff through pipes, gutters, and channels. Conveyance elements are described by slope, length, hydraulic roughness, and cross section dimensions.
- **Confluence Elements** Confluence elements are used to combine runoff hydrographs. Confluences are described by a single value which defines the number of hydrographs to be combined.

• **Detention Basin Elements** - Detention basin elements route runoff through a detention basin. Detention basin elements are described numerically by a stage-volume relationship, a stage discharge relationship, and an initial water level.

The model also includes unit detention basins which modify the runoff hydrographs from subbasins where runoff is restricted to a peak discharge (see Figure I). The basic stage-volume and stage-discharge relationships for the unit detention basin were calculated to limit the peak runoff flow rate to 0.2 cfs per acre. Unit detention basins produce a runoff hydrograph with a peak flow rate that is approximately equal to the area of the upstream subbasin multiplied by 0.2 cfs. Unit detention basins do not represent an actual facility, but rather the approximate performance of local detention facilities located at individual developments within the subbasin.

• **Connectivity Data** - Connectivity data defines the order in which the model elements are processed by HEC-1. Each model element is assigned a rank and the HEC-1 input file is written according to that rank. The order in which model elements are processed by HEC-1 establishes hydrograph routing and when hydrographs are combined.

# **Model Tools**

All of the data associated with the model elements are contained within the GIS database. HMI accesses the GIS database, calculates hydrologic characteristics of the subbasins, and assembles the data to create input files for HEC-1. Input files are processed by HEC-1 to calculate the runoff hydrographs. Runoff hydrographs are calculated for subbasins, conveyances, confluences, and detention basins. HMI can then read the HEC-1 hydrograph files, identify peak flowrates, and write the hydrograph data to the GIS database. Some of the tools used to accomplish these tasks are as follows:

- **Connectivity Editor** This tool allows the user to define hydrograph routing by assigning a rank to each of the model elements. The rank establishes the order that the element is written to the HEC-1 file. When a new element is inserted into the model, this tool automatically adjusts the rank of the subsequent elements.
- **Subbasin Analysis -** This tool uses information from the GIS database to calculate subbasin area, the percentages of connected and unconnected impervious area, and the representative SCS curve number for each subbasin.
- **HEC-1 Input File Writer** The HEC-1 input file writer gathers the model data from the GIS database and writes the input file that is used by HEC-1 to calculate the runoff hydrographs.

#### **Modeling Existing Conditions**

The existing storm drain system was modeled as accurately as possible given the available information and resources. Not all existing pipes, ditches, and gutters are included in the model, but major storm drainage facilities and features are represented in the model. Many of the smaller facilities are represented in the characteristics of the subbasins. The model was used to identify existing inadequacies in the storm drain system and to serve as a base to develop the future model.

#### **Modeling Future Conditions**

A model of the future storm drainage system was prepared to assist with development of a preferred drainage plan for the area of Riverton City west of Bangerter Highway. Drainage plan alternatives were modeled and then refined until a preferred drainage plan was developed. The development of the preferred drainage plan is described in the following section. The future system was modeled with anticipated land use at buildout conditions. Land use and hydrologic characteristics in existing developed areas were assumed to remain the same. Future land use and hydrologic characteristics in currently undeveloped areas were estimated for a buildout condition based upon current zoning and land use provided by Riverton City.

Regional detention facilities are required to detain runoff from a 100-year storm event and release at a rate of 0.2 cfs per acre –. The first exception area is roughly between 13000 South and 13400 South and between 4300 West and 5000 West (see Figure I). This area is required to detain runoff from a 100-year storm event and release at a rate of 0.1 cfs per acre. Western Springs is the second exception area. It is located between 12600 South and 13000 South and 4570 West and 5000 West (see Figure I). This area is required to detain runoff from a 100-year storm event and release at a maximum flow rate of 5 cfs. These two exception areas require larger detention facilities and smaller release rates to compensate for conveying historical storm runoff from Butterfield Creek to Midas Creek and Rose Creek. Flow rates from any storm up to a 100-year event cannot be higher than the historical peak flow rates reported in the 2002 Salt Lake County Southwest Creek and Canal Study. The duration of the 100-year storm event used to size the detention facility should be the duration that produces the largest volume of runoff in the detention facility given the required release rate.

It is assumed in the future conditions model that runoff is detained to 0.2 cfs per acre – with the exception of two areas. The first exception area is roughly between 13000 South and 13400 South and between 4300 West and 5000 West (see Figure I). Runoff in this area was detained to a rate of 0.1 cfs per acre. Western Springs is the second exception area. It is located between 12600 South and 13000 South and 4570 West and 5000 West (see Figure I). Runoff in this area was detained to a flow of 5 cfs.

#### **Computation of Runoff Hydrographs**

Hydrographs were computed for each subbasin, conveyance, confluence, detention basin inlet, and detention basin outlet. The maximum value from each hydrograph is the peak runoff flow

rate. HMI determines the peak runoff flow rate for each hydrograph and adds the hydrographs to the GIS database. Hydrographs were calculated for the 1-hour, 3-hour, and 6-hour storm duration. The highest peak flow rate identifies the critical storm duration and is the flow rate used for design or evaluation of that element of the model. Elements in the future drainage system were designed for the 10-year storm event and the critical storm duration.

As the drainage plan for the future system was developed, runoff hydrographs were calculated for various alternatives. The peak flowrates were then compared to the capacities of the model elements to determine where additional refinements were needed. Peak runoff flowrates for each conveyance and other model elements are provided in Appendix A. The location of each conveyance by element connectivity number is illustrated on Figure II.

# **CHAPTER IV**

## **IMPLEMENTATION PLAN**

This Chapter contains a discussion of the actions Riverton City staff and HAL recommends be implemented to improve the storm drainage system in the study area. The following topics are included in this section:

- Master Plan Projects
- Estimated Construction Costs of Master Plan Projects
- Funding Sources
- Maintenance
- Storm Drainage Policies
- Summary of Recommendations

### MASTER PLAN PROJECTS

Meetings were held with Riverton City personnel to evaluate alternatives for the storm drainage plan west of Bangerter Highway. Selection of the preferred alternative was a process of evaluation and refinement, rather than a simple choice between alternatives. Riverton City personnel efficiently eliminated impractical solutions and formulated practical solutions. The process of selecting a preferred alternative by City staff included: reviewing the recent flooding problems and storm drainage inadequacies, brainstorming possible solutions to the problems, screening alternatives based on feasibility and public acceptance, development of alternatives, comparison based on cost and function, and selection of the preferred alternative. The preferred alternatives are the master plan improvement projects.

#### **Master Plan Projects Description**

The overall goal of the master plan projects is to convey storm runoff to Midas Creek or Rose Creek away from Butterfield Creek and the Provo Reservoir Canal. Flow historically tributary to Butterfield Creek will need to be conveyed to Midas Creek and Rose Creek. Commercial developments are required to have an on-site detention facility to detain runoff from a 100-year storm event and release at a rate of 0.2 cfs per acre. Storm runoff from residential developments is required to be detained in regional or local detention facilities (see Figure I). Residential developments not located within an area of a regional detention facility are required to have an on-site detention facility to detain of 0.2 cfs per acre. The duration of the 100-year storm event used to size a detention facility should be the duration that produces the largest volume of runoff in the detention facility given the allowable release rate. In addition, both commercial and residential development are to accommodate or identify a safe route for a storm event larger than a 100-year storm event.

Regional detention facilities are required to detain runoff from a 100-year storm event and release at a rate of 0.2 cfs per acre – with the exception of two areas. The first exception area is roughly between 13000 South and 13400 South and between 4300 West and 5000 West (see Figure I). This area is required to detain runoff from a 100-year storm event and release at a rate of 0.1 cfs per acre. Western Springs is the second exception area. It is located between 12600 South and 13000 South and 4570 West and 5000 West (see Figure I). This area is required to detain runoff from a 100-year storm event and release at a maximum flow rate of 5 cfs. These two exception areas require larger detention facilities and smaller release rates to compensate for conveying historical storm runoff from Butterfield Creek to Midas Creek and Rose Creek. Flow rates from any storm up to a 100-year event cannot be higher than the historical peak flow rates reported in the 2002 Salt Lake County Southwest Creek and Canal Study. The duration of the 100-year storm event used to size the detention facility should be the duration that produces the largest volume of runoff in the detention facility given the required release rate. In addition to accommodate or identify a safe route for a storm event larger than a 100-year storm event.

# **Estimated Construction Costs for Master Plan Projects**

Estimated construction costs for the storm drainage pipe lines include manholes and inlets. It was assumed most of these projects are not located in roads or in new development and do not include costs for repairs, replacing, or relocating existing road features. Estimated construction costs for detention facilities include excavation, grading, low flow pipes, inlet and outlet structures, irrigation systems, general landscaping, and land cost.

Unit costs for the construction cost estimates are based on conceptual level engineering. Sources used to estimate construction costs include:

- 1. "Means Heavy Construction Cost Data, 2004"
- 2. Price quotes from equipment suppliers
- 3. Recent construction bids for similar work

All costs are presented in 2004 dollars. Recent price and economic trends indicate that future costs are difficult to predict with certainty. Engineering cost estimates given in this study should be regarded as conceptual level as appropriate for use as a planning guide. Only during final design can a definitive and more accurate estimate be provided. Table IV-1 is a unit pipe cost table with assumptions used in calculating an estimated cost for each project. A detailed cost estimate of each project is provided in Appendix C.
DIAMETER (IN)	COST PER FOOT
15	\$50
18	\$61
21	\$66
24	\$73
27	\$84
30	\$95
36	\$116
42	\$135
48	\$158
54	\$186

TABLE IV-1PIPE COST ASSUMPTIONS FOR STORM DRAIN MASTER PLAN PROJECTS

The projects are listed in Table IV-2. The location of each project is shown on Figure III by project "ID" number. The flows and pipe diameters given in Table IV-2 are approximate and are for planning purposes only. A detailed hydraulic analysis should be performed during the design process for the master plan improvement projects to identify final design pipe sizes.

TABLE IV-2STORM DRAINAGE MASTER PLAN PROJECTS

ID	DESCRIPTION <sup>1</sup>	ESTIMATED COST <sup>2</sup>
1	Modify the retention pond at about 4570 W and Goshute with an outlet structure. Also, install 4500 feet of 24 inch diameter pipe to convey 22 cfs from the retention pond north in 4570 W to 12600 S and east in 12600 S to 4000 W. Install 2350 feet of 30 inch diameter pipe to convey 27 cfs from 12600 S and 4000 W north in 4000 W to about Swensen Farms Dr.	\$937,000
2	Install 1,400 feet of 21 inch diameter pipe to convey 7 cfs from about 13600 S to Rose Creek and 13400 S to Rose Creek in 4600 S.	\$126,000
3	Install 1,550 feet of 42 inch diameter pipe to convey 135 cfs from about 4600 W to Master Plan Project ID 4 detention basin in about 13200 S.	\$286,000

# TABLE IV-2 STORM DRAINAGE MASTER PLAN PROJECTS (Continued)

ID	DESCRIPTION <sup>1</sup>	ESTIMATED COST <sup>2</sup>
4	Construct an 8 acre-ft detention basin at about 4400 W and 13200 S and install 2,500 feet of 30 inch diameter pipe to convey 20 cfs from the detention basin to Rose Creek.	\$734,000
5	Install 1,600 feet of 30 inch diameter pipe to convey 29 cfs from about 5100 W in 13400 S to Master Plan Project ID 14 detention basin.	\$202,000
6	Install 2,500 feet of 30 and 36 inch diameter pipe to convey 50-70 cfs from about 4800 W to 5200 W in about 13600 S.	\$359,000
7	Install 1,600 feet of 30 inch diameter pipe to convey 23 cfs in 4600 W from about 13000 S to 13200 S.	\$207,000
8	Install 2,000 feet of 18 and 24 inch diameter to convey 7-15 cfs from about 4000 W and 13200 S to Rose Creek.	\$110,000
9	Install 1400 feet of 27 and 30 inch diameter pipe and a 1.5 acre-ft detention basin at about 4000 W and 12300 S.	\$309,000
10	Install 3,150 feet of 42 and 48 inch diameter pipe from about 4000 W and 13000 S to Rose Creek at about 13500 S and 3900 W.	\$623,000
11	Install 3,500 feet of 30 and 36 inch diameter pipe to convey 42-50 cfs from 3900 W and 13650 S to 3600 W and Rose Creek.	\$531,000
12	Install 1,800 feet of 36 inch diameter pipe to convey 75 cfs from 4600 W to 4800 W at about 13200 S.	\$285,000
13	Install 1,150 feet of 21 inch diameter pipe to convey 4-7 cfs from about 11800 S to Midas Creek in 4000 W.	\$104,000
14	Construct a 5 acre-ft detention basin at about 4800 W and 13600 S.	\$410,000
15	Install 1,000 feet of 18 and 24 inch diameter pipe and a 1 acre-ft detention basin at about 4130 W and 11900 S to Midas Creek.	\$160,000
16	Construct a waste way at Midas Creek and the Provo Reservoir Canal.	\$14,000
17	Install 1,200 feet of 21 inch diameter to convey 10 cfs from 13400 S and 4500 W to Rose Creek	\$108,000
18	Install 1,000 feet of 18 inch diameter pipe to convey 10 cfs from 4000 W and 12700 S to 12600 S and Bangerter Highway	\$83,000

## TABLE IV-2 STORM DRAINAGE MASTER PLAN PROJECTS (Continued)

ID	DESCRIPTION <sup>1</sup>	ESTIMATED COST <sup>2</sup>
19	Install 3,000 feet of 18 and 30 inch diameter pipe to convey 7-34 cfs from 4400 W to 3950 W at about 13000 S.	
20	20 Install 1,000 feet of 18 inch diameter pipe to convey 4 cfs from 12800 S to 13000 S in 4400 W.	
21	Install 1,300 feet of 18 inch diameter pipe to convey 9 cfs from about 4300 W and 12800 S to 4200 W and 13000 S.	\$108,000
22	Install 1,600 feet of 18 inch diameter pipe to convey 5 cfs in 4100 W from 12700 S to 13000 S.	\$133,000
23	Install 700 feet of 21 inch diameter pipe to convey 9 cfs at about 3950 W from 12800 S to 13000 S.	\$63,000
24	Install 1,000 feet of 36 inch diameter pipe in 4300 W from 12350 S to 12200 S.	\$158,000
25	Construct a waste way at Rose Creek and the Provo Reservoir Canal.	\$14,000
	TOTAL	\$6,474,000

1) The flows and pipe diameters given are approximate and are for planning purposes only. A detailed hydraulic analysis should be performed during the design process for the master plan improvement projects to identify final design pipe sizes.

2) Estimated construction costs include manholes, inlets, contingency, and engineering. Costs are in 2004 dollars.

## FUNDING SOURCE OPTIONS

Riverton City has the option to expand its authority as a Utah Municipal Corporation to establish a Storm Water Utility. Under this authority, the City can establish funding mechanisms necessary to support planned storm water system improvements as well as the day to day operations and maintenance of the existing system. The funding options available are similar to those established for other municipal utility functions. The flexibility established in Utah Code for sanitary sewers (and therefore for storm sewers) allows the City access to most generally accepted methods of public infrastructure financing. These funding options could include general obligation bonds, revenue bonds, State/Federal grants and loans, impact fees, and storm water management service charges (a Storm Water Utility). In reality, the City may need to consider a combination of these funding options. The following discussion describes each of these options.

## **General Obligation Bonds**

This form of debt enables the City to issue general obligation bonds for capital improvements and replacement. General Obligation (G.O.) Bonds are debt instruments backed by the full faith and credit of the City which would be secured by an unconditional pledge of the City to levy assessments, charges or ad valorem taxes necessary to retire the bonds. G.O. bonds are the lowest-cost form of debt financing available to local governments and can be combined with other revenue sources such as specific fees, or special assessment charges to form a dual security through the City's revenue generating authority. These bonds are supported by the City as a whole, so the amount of debt issued for storm water is limited to a fixed percentage of the real market value for taxable property within the City.

## **Revenue Bonds**

This form of debt financing is also available to the City for utility related capital improvements. Unlike G.O. bonds, revenue bonds are not backed by the City as a whole, but constitute a lien against the storm water service charge revenues of a Storm Water Utility. Revenue bonds present a greater risk to the investor than do G.O. bonds, since repayment of debt depends on an adequate revenue stream, legally defensible rate structure /and sound fiscal management by the issuing jurisdiction. Due to this increased risk, revenue bonds generally require a higher interest rate than G.O. bonds. This type of debt also has very specific coverage requirements in the form of a reserve fund specifying an amount, usually expressed in terms of average or maximum debt service due in any future year. This debt service is required to be held as a cash reserve for annual debt service payment to the benefit of bondholders. Typically, voter approval is not required when issuing revenue bonds. In addition, revenue bonding for a storm water program that has a limited track record may be problematic. The bond underwriters may have some concerns regarding the viability of a relatively new program and its legal defensibility. Therefore, a city that is just starting out may need to use G.O. bonds at first, until a track record is established.

## State/Federal Grants and Loans

Historically, both local and county governments have experienced significant infrastructure funding support from state and federal government agencies in the form of block grants, direct grants in aid, interagency loans, and general revenue sharing. Federal expenditure pressures and virtual elimination of federal revenue sharing dollars are clear indicators that local government may be left to its own devices regarding infrastructure finance in general and storm water funding in particular. However, state/federal grants and loans should be further investigated as a possible funding source for needed storm water improvements.

It is also important to assess likely trends regarding federal / state assistance in infrastructure financing. Where federal mandate for sanitary sewer improvements in the 1960's was accompanied by a very generous and available grant program, future trends indicate that grants will be replaced by loans through a public works revolving fund. Local governments can expect to access these

revolving funds or public works trust funds by demonstrating both the need for and the ability to repay the borrowed monies, with interest. As with the revenue bonds discussed earlier, the ability of infrastructure programs to wisely manage their own finances will be a key element in evaluating whether many secondary funding sources, such as federal/state loans, will be available to the City's storm water management program.

## **Impact Fees**

Impact fees can be applied to drainage related facilities under the Utah Impact Fees Act. The Utah Impacts Fees Act is designed to provide a logical and clear framework for establishing new development assessments. It is also designed to establish the basis for the fee calculation which the City must follow in order to comply with the statute. However, the fundamental objective for the fee structure is the imposition on new development of only those costs associated with providing or expanding storm water infrastructure to meet the capacity needs created by that specific new development. Also, impact fees cannot be applied retroactively.

There are significant areas of potential development within the Riverton City study area. Development of these areas could represent a significant source of revenue through the assessment of a storm water impact fee. The impact fee must be calculated such that it will represent a fair and equitable allocation of cost to proposed storm drainage facilities based on impacts to those facilities from the new development areas. Impact fees generated from new development will not pay for all of the costs of the needed drainage facilities. Existing development within the City is also contributing to the required sizing of these facilities. Therefore, the impact fees must be determined by taking into consideration what portion of the proposed facilities is required due to new development versus what portion is required due to existing development.

## Storm Water Management Service Charges (Storm Water Utility)

As conventional funding sources for storm water management become more difficult to access and as federal (Environmental Protection Agency - National Pollutant Discharge Elimination System) and state storm water quality requirements become mandatory, the utility approach toward funding is becoming generally accepted. There are numerous combinations and variations for storm water service charges. The City could employ an equivalent service unit (ESU) approach which is based on measured impervious surface. Because most single family residents have very similar impervious surface footprints, all single family homes are considered to be one ESU. All other properties are charged based on their measured impervious surface area divided by the base ESU square footage to determine the number of ESU's applied to that property.

## MAINTENANCE

It is impossible to overstate the importance of effective maintenance in the overall storm water management effort. Without maintenance, drainage facilities will deteriorate, and their design capacities will be reduced by accumulations of sediments, weeds and debris. Not only will they fail

to function as intended, but they will become hazards and a blight on the City's landscape. Inadequate maintenance, as with any facility, transforms a productive resource into a multi-faceted liability. Storm drainage facilities within the city have historically been well maintained. The City's public works staff has done an excellent job of prioritizing and implementing maintenance activities.

The construction of additional facilities in the future increases the maintenance burden. Existing and future operating costs need to be addressed as part of an overall financial analysis of the storm drain system. It is imperative that sufficient maintenance manpower and equipment are made available to ensure proper function and community acceptance.

## STORM DRAINAGE ORDINANCE AND DESIGN STANDARDS

Responsibilities regarding the Storm Drainage Plan should be incorporated into City design standards and/or ordinances. The City has the responsibility of implementing the Storm Drainage Master Plan. However, developers must also assume responsibility for conforming to the requirements of the Storm Water Master Plan. It is the developer's responsibility to comply with runoff restrictions, to show that the storm runoff which is generated upstream from the development can be conveyed through the development, and to demonstrate that runoff generated by the proposed development will not increase the impact of drainage waters on downstream property owners.

It is important that existing and future developments comply with runoff restrictions. Existing and future storm drain facilities were evaluated in the storm drain model assuming the allowable runoff restrictions will be achieved with detention facilities. If detention facilities are not constructed or properly maintained, runoff flowrates will exceed the capacity of the existing or future facilities. It is recommended that the City continue the design review and inspection practices that will ensure that runoff restrictions are met. The City should consider adopting the recommended site development storm drainage and erosion control plan submittal requirements included in Appendix D.

## RECOMMENDATIONS

- 1. The City should proceed with following the recommendations made in this report and construct the storm drainage master plan projects as the area of Riverton City west of Bangerter Highway develops. The City should also follow the recommendations made in the 2002 Salt Lake County Southwest Creek and Canal Study.
- 2. Model data should be updated as land use, conveyance, capacity, and detention are modified or constructed.
- 3. Commercial developments shall be required to detain their own runoff. Residential developments shall be required to detain their own runoff or be required to detain the runoff in a regional detention facility as appropriate for the location (see Figure I).

- 4. Regional and local detention facilities shall be designed to detain storm runoff from a 100year event and released at 0.1 cfs per acre, 0.2 cfs per acre, or 5 cfs as appropriate for the location (see Figure I). The duration of the 100-year storm event used to size the detention facility shall be the duration that produces the largest volume of runoff in the detention facility given the required release rate. All storm drain outfalls to Midas Creek or Rose Creek shall be approved by Salt Lake County Flood Control.
- 5. The City should consider adopting the site development storm drainage and erosion control plan submittal requirements included in Appendix D.

## REFERENCES

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## **APPENDIX A**

STORM DRAINAGE MODEL OUTPUT

## STORM DRAINAGE MODEL CONNECTIVITY AND PEAK FLOW

ORDER	HMI ID	TYPE	PEAK (CFS)
1	SB69	Subbasin	5.7
2	CV34	Conveyance	5.7
3	CV35	Conveyance	5.6
4	SB59	Subbasin	12.5
5	HC24	Confluence	12.5
6	CV36	Conveyance	12.5
7	SB56	Subbasin	10.8
8	HC25	Confluence	22.9
9	CV10	Conveyance	22.9
10	CV11	Conveyance	22.8
11	SB66	Subbasin	20.6
12	CV37	Conveyance	20.5
13	SB77	Subbasin	22.6
14	HC26	Confluence	41.5
15	CV9	Conveyance	41.1
16	SB55	Subbasin	14.3
17	HC7	Confluence	55.5
18	CV12	Conveyance	55.2
19	SB57	Subbasin	13.6
20	HC8	Confluence	88.8
21	CV13	Convevance	88.7
22	DB2	Detention	9.8
23	CV16	Convevance	9.7
24	SB60	Subbasin	21.7
25	DB3	Detention	0.5
26	CV14	Convevance	0.5
27	SB58	Subbasin	22.5
28	HC10	Confluence	22.5
29	CV15	Convevance	22.3
30	HC9	Confluence	22.4
31	CV19	Convevance	22.4
32	SB63	Subbasin	9.1
33	SB28	Subbasin	5.5
34	SB27	Subbasin	8.8
35	SB26	Subbasin	21.7
36	SB25	Subbasin	23.6
37	HC38	Confluence	54.5
38	CV42	Convevance	54.5
39	CV41	Convevance	54.5
40	CV38	Convevance	54.5
41	CV39	Conveyance	54.5
42	SB36	Subbasin	13.5
43	HC18	Confluence	55.8
44	CV40	Convevance	55.8
45	DB5	Detention	33.5
46	SB34	Subbasin	2.0
47	SB33	Subbasin	11.1
48	HC13	Confluence	13.1
49	CV21	Conveyance	13.1

ORDER	HMI ID	TYPE	PEAK (CFS)
50	SB35	Subbasin	9.5
51	HC14	Confluence	22.5
52	CV22	Conveyance	22.2
53	DB4	Detention	0.5
54	CV23	Conveyance	0.5
55	HC27	Confluence	34.0
56	CV18	Conveyance	32.2
57	CV100	Conveyance	30.3
58	SB113	Subbasin	29.4
59	CV104	Conveyance	28.9
60	SB30	Subbasin	21.3
61	SB111	Subbasin	36.3
62	HC80	Confluence	50.0
63	CV102	Convevance	50.0
64	SB112	Subbasin	22.5
65	HC73	Confluence	68.4
66	CV103	Conveyance	68.5
67	HC79	Confluence	94.1
68	DB16	Detention	18.2
69	HC12	Confluence	58.7
70	CV101	Conveyance	56.9
71	SB110	Subbasin	23.7
72	CV105	Conveyance	6.6
73	SB118	Subbasin	10.1
70	HC71	Confluence	61.6
75	CV20	Conveyance	59.6
76	SB72	Subbasin	62.4
77	HC28	Confluence	71.0
78	CV95	Conveyance	70.5
79	SB75	Subbasin	56.3
80	CV88	Conveyance	56.4
81	CV89	Conveyance	56.1
82	SB45	Subbasin	6.8
83	DB6	Detention	1.0
84	SB29	Subbasin	24.0
85	HC78	Confluence	24.0
86	CV91	Conveyance	23.1
87	SB73	Subbasin	63.1
88	HC63	Confluence	135.6
89	CV90	Conveyance	135.3
90	SB103	Subbasin	26.8
<u>91</u>	HC64	Confluence	155.4
97	DB13	Detention	10 3
02	CV50	Conveyance	10.0
93 94	SB99	Subbasin	31.5
0 <del>4</del> 05	HC67	Confluence	95.0
90	CV52	Conveyance	03.0
07	SR93	Subhasin	33.9
07 08	CV93	Conveyance	6.0
00	SR94	Subhasin	37.2
99 100	HC65	Confluence	1/ 2
100	CV94	Conveyance	14.3
107	HC51	Confluence	104.2
102		3011100100	107.2

ORDER	HMI ID	TYPE	PEAK (CFS)
103	CV71	Conveyance	103.2
104	SB98	Subbasin	33.9
105	SB49	Subbasin	8.8
106	CV24	Conveyance	3.7
107	SB48	Subbasin	8.3
108	HC55	Confluence	7.3
109	CV64	Conveyance	7.4
110	SB117	Subbasin	17.4
111	SB88	Subbasin	13.2
112	HC23	Confluence	8.7
113	CV114	Conveyance	8.7
114	SB91	Subbasin	53.6
115	SB89	Subbasin	39.3
116	HC45	Confluence	31.1
117	CV65	Conveyance	31.1
118	SB107	Subbasin	8.8
119	CV97	Convevance	2.5
120	CV98	Conveyance	2.5
121	HC68	Confluence	33.4
122	CV99	Conveyance	33.4
123	SB90	Subbasin	45.4
120	CV66	Conveyance	9.2
124	HC46	Confluence	42.5
120	CV67	Conveyance	42.5
120	SB02	Subbasin	36.7
127	SB10/	Subbasin	24.5
120		Confluence	54.3
129		Conveyance	54.3
130	SB105	Subbasin	15 5
131	HC18	Confluence	57.2
132		Conveyance	57.1
134	SB106	Subbasin	1/1 3
134		Confluence	60.8
135	CV70	Conveyance	60.7
130		Confluence	60.3
137	CV/79	Convoyance	09.3 60.3
130	SD40	Subbosin	12.2
139		Detention	10.0
140		Convoyonoo	1.2
141	SB30	Subbasin	1.2
142	SB33	Subbasin	12.1
143		Confluence	10.9
144	01/26	Convoyonas	∠J. I
140	CV20 CD27	Subbasia	22.8
140	SD31	Convoyonas	9.1
14/	CV00 CD00	Subbooin	9.1
148	3030 UC25	Confluence	10.2
149		Convoyerse	10.8
150	0VZ1	Subbosin	10.4
151	3043 UC22	Confluence	5.9
152		Connuence	45.7
153		Conveyance	45.3
154	3844		12.0
155	1030	Comuence	55.7

ORDER	HMI ID	TYPE	PEAK (CFS)
156	CV29	Conveyance	55.3
157	SB46	Subbasin	3.9
158	HC33	Confluence	59.2
159	CV30	Conveyance	58.7
160	SB42	Subbasin	1.2
161	HC34	Confluence	58.9
162	DB8	Detention	3.5
163	CV119	Conveyance	3.4
164	SB76	Subbasin	13.2
165	SB47	Subbasin	10.8
166	HC37	Confluence	17.6
167	CV55	Convevance	17.6
168	SB84	Subbasin	14.7
169	HC20	Confluence	21.6
170	CV79	Conveyance	21.6
171	CV61	Conveyance	21.5
172	SB82	Subbasin	38.9
173	HC82	Confluence	26.6
176	CV84	Conveyance	26.5
174	SB81	Subbasin	18.8
176	CV59	Conveyance	18.0
170	SB78	Subbasin	23.0
178	CV/86	Conveyance	20.0
170	SB80	Subbasin	17.8
179		Confluence	57.5
100		Dotontion	12.7
101	CV85	Conveyance	13.7
102		Confluence	35.8
103	CV/58	Conveyance	34.8
104	SB116	Subbasin	5.2
100		Confluence	35.8
100	CV57	Conveyance	35.0
107	SB115	Subbasin	10.0
180	CV/100	Conveyance	19.0
109		Confluence	30.0
190	CV/117	Conveyance	39.0
191	SP6	Subbasin	39.0
192	000 CV/5	Conveyance	4.9
193	CV6	Conveyance	4.0
194	CV0 CP2	Subbasin	4.0
195		Subbasin	7.2
190		Confluence	7.3
197		Coniluence	21.0
190		Conveyance	21.2
199	303	Subbasin	1.0
200		Conveyence	22.4
201	0VZ	Subbooin	22.3
202	3D/ 8DE	Subbasin	10.0
203	9R2		10.0
204		Continuence	32.0
205	CV4	Conveyance	31.0
206	5B4	Subbasin	3.8
207		Coniluence	34.4
208	643	Conveyance	34.1

ORDER	HMI ID	TYPE	PEAK (CFS)
209	HC3	Confluence	54.4
210	DB1	Detention	9.2
211	CV7	Conveyance	9.2
212	SB50	Subbasin	6.5
213	DB9	Detention	0.2
214	CV31	Conveyance	0.2
215	SB51	Subbasin	7.4
216	HC16	Confluence	15.3
217	CV33	Conveyance	15.3
218	CV110	Conveyance	15.3
219	SB114	Subbasin	19.4
220	CV115	Conveyance	19.3
221	DB14	Detention	4.6
222	CV116	Conveyance	4.6
223	SB100	Subbasin	13.5
224	HC83	Confluence	23.6
225	CV118	Conveyance	23.6
226	HC61	Confluence	62.3
227	CV111	Conveyance	62.3
228	SB101	Subbasin	20.5
229	SB86	Subbasin	7.3
230	HC59	Confluence	68.1
231	CV112	Conveyance	68.1
232	SB79	Subbasin	6.1
233	CV82	Conveyance	1.7
234	SB83	Subbasin	17.8
235	CV83	Conveyance	5.0
236	SB108	Subbasin	15.6
237	CV62	Conveyance	4.4
238	SB85	Subbasin	6.2
239	SB87	Subbasin	11.1
240	HC44	Confluence	9.3
241	CV60	Conveyance	9.3
242	SB96	Subbasin	42.4
243	CV72	Conveyance	42.3
244	CV76	Conveyance	41.7
245	SB97	Subbasin	14.4
246	SB95	Subbasin	44.1
247	HC54	Confluence	49.4
248	CV73	Conveyance	49.6
249	CV75	Conveyance	49.3

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THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY, DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

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5 IO	1									
6 КК	SB69									
7 BA	1.09									
8 PB	0.875									
9 IN	1									
10 PI	0.000	0.000	0.002	0.002	0.002	0.002	0.002	0.002	0.003	0.003
11 PI	0.004	0.005	0.008	0.009	0.009	0.013	0.017	0.02	0.024	0.029
12 PI	0.033	0.034	0.035	0.038	0.039	0.045	0.052	0.054	0.054	0.054
13 PI	0.052	0.045	0.04	0.035	0.03	0.022	0.02	0.018	0.016	0.014
14 PI	0.012	0.011	0.01	0.009	0.009	0.008	0.006	0.006	0.005	0.005
15 PI	0.005	0.005	0.004	0.004	0.004	0.003	0.003	0.002	0.002	0.001
16 LS	0	65	0.1							
17 UD	1.00									
18 KO					22					
19 КК	CV34									
20 RD	306.052	0.02000	0.015		CIRC	3.50	0.00			
21 КО					22					
22 КК	CV35									
23 RD	605.262	0.04800	0.015		CIRC	3.00	0.00			
24 ко					22					
25 КК	SB59									
26 BA	0.0297									
27 LS	0.1	98.000			76.756	0.1				
28 UK	25	.02	.1	27.24						
29 UK	60	.02	. 4	72.76						
30 RD	600	.01	.02		TRAP	2	25			
31 КО					22					
32 КК	HC24									
33 HC	2									
34 КО					22					
35 КК	CV36									
36 RD	558.153	0.01000	0.015		CIRC	4.00	0.00			
37 КО					22					
38 КК	SB56									
39 BA	0.0290									
40 LS	0.1	98.000			77.049	0.1				
41 UK	2 5	.02	0.1	25.69						
42 UK	60	.02	.04	74.31						
43 RD	400	.01	.02	.005	TRAP	2	25			
4.4 RD	2300	.01	.015		CIRC	1.25				
45 KO					22					

PAGE 2

LINE	ID	1	2.	3.	4.	5	6	7	8	910
46	КK	HC25								
47	HC	2								
48	KO					22				
49	KK	CV10								
50	RD	922.974	0.01000	0.015		CIRC	4.00	0.00		
51	KO					22				
52	KK	CV11								
53	RD	275.246	0.01000	0.015		CIRC	4.50	0.00		
54	KO					22				
55	KK	SB66								
56	BA	0.0550								
57	LS	0.1	98.000			78.152	0.1			
58	UK	25	0.02	0.1	24.84					
59	UK	60	0.02	0.4	75.16					
60	RD	400	.01	.02	0.005	TRAP	2	25		
61	RD	1500	.01	.015		CIRC	1.25			
62	KO					22				
63	KK	CV37								
64	RD	1375.48	0.01000	0.015		CIRC	3.00	0.00		
65	KO					22				
66	KK	SB77								
67	BA	0.0604								
68	LS	0.1	98.000			75.000	0.1			
69	UK	25	.02	.1	25.00					
70	UK	60	.02	. 4	75.00					
71	RD	1000	.01	.02		TRAP	2	25		
72	KO					22				
73	KK	HC26								
74	HC	2								
75	KO					22				
76	ΚK	CV9								
77	RD	433.758	0.04200	0.015		CIRC	2.50	0.00		
78	KO					22				
79	ΚK	SB55								
80	BA	0.0400								
81	LS	0.1	98.000			77.272	0.1			
82	UK	2 5	.02	.1	24.31					
83	UK	60	.02	. 4	75.69					
84	RD	500	.01	.02	.005	TRAP	2	25		
85	RD	1800	.01	.015		CIRC	1.5			
86	KO					2.2				

#### PAGE 3

LINE	ID.	1	2.		4.		6	7	8	9	10	
87	КK	HC7										
88	HC	2										
89	KO					22						
90	KK	CV12										
91	RD	640.004	0.04000	0.015		CIRC	3.00	0.00				
92	KO					22						
93	KK	SB57										
94	BA	0.0465										
95	LS	0.1	98.000			70.952	0.1					
96	UK	25	.02	.1	18.88							
97	UK	60	.02	. 4	81.12							
98	RD	500	.01	.02		TRAP	2	25				
99	KO					22						
100	KK	HC8										
101	HC	3										
102	KO					22						
103	KK	CV13										
104	RD	96.377	0.01000	0.015		CIRC	4.50	0.00				
105	KO					22						
106	кк	DB2										
107	RS	000	FLOW									
108	SV	0	1 1 1	2	З	4	5	6	7	8	9	
109	SE	0	0.5	1	1.5	2	2.5	3	3.5	4	4.5	
110	so	0	1	2	8	10	2.0	23	27	3.0	60	
111	KO					22						
110	14.14	01110										
112	R R R R R R R R R R R R R R R R R R R	1070 21	0 0 2 0 0 0	0 015		CIDC	2 50	0 00				
114	KO	1919.21	0.03000	0.015		22	2.30	0.00				
114	RO					22						
115	ΚK	SB60										
116	BA	0.0797										
117	LS	0.1	98.000			72.246	0.1					
118	UK	25	.02	.1	18.43							
119	UK	60	.02	. 4	81.57							
120	RD	800	.01	.02	.05	TRAP	2	25				
121	RD	1500	.01	.015		CIRC	1.25					
122	KO					22						
123	KK	DB3										
124	RS		FLOW									
125	SV	0	0.5	1	1.5	2	2.5	3	4			
126	SE	0	0.5	1	1.5	2	2.5	3	4			
127	SQ	0	0.25	0.5	1	2	4	5	25			
128	KO					22						

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## LINE ID.....1.....2......3.....4......5.....6......7......8......9.....10

129	ΚK	CV14						
130	RD	1167.79	0.01000	0.015		CIRC	2.25	0.00
131	KO					22		
132	КК	SB58						
133	D 7	0 0678						
124	DA I C	0.00/0	00 000			70 002	0 1	
134	10	0.1	90.000	1	2.2 6.1	78.005	0.1	
135	UK	25	.02	• 1	22.61			
136	UK	60	.02	. 4	//.39			
137	RD	900	.02	.02	.005	TRAP	2	25
138	RD	825	.025	.015		CIRC	2	
139	KO					22		
140	ΚK	HC10						
141	HC	2						
142	KO					22		
143	ΚK	CV15						
144	RD	212.594	0.01000	0.015		CIRC	3.00	0.00
145	КО					22		
146	КK	HC9						
147	HC	2						
148	КО					2.2		
149	КК	CV19						
150	RD	1390.35	0.02240	0.015		CIRC	3.00	0.00
151	КO					22		
152	КК	SB63						
153	BA	1 19						
154	тс	1.15	6.5	0 1				
155	10	0 55	05	0.1				
155	UD KO	0.55				2.2		
100	ко					22		
1 5 7		9500						
157	nn D2	5828						
150	BA	0.72	<i>c</i> =	0 1				
123	ĹS	0	65	0.1				
160	UD	0.55						
161	KO					22		
162	ΚK	SB27						
163	BA	1.30						
164	LS	0	67	0.1				
165	UD	1.36						
166	KO					22		
167	ΚK	SB26						
168	BA	0.43						
169	LS	0	74	0.1				
170	UD	0.37						
171	KO					22		

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LINE	ID	1	2.	3.	4 .		6	7	8	9	10
172	кк	SB25									
173	BA	0 53									
174	LS	0.00	74	0 1							
175		0 56	/ 4	0.1							
176	UD KO	0.50				2.2					
1/0	KŬ					22					
177	ΚK	HC38									
178	HC	5									
179	KO					22					
180	ΚK	CV42									
181	RD	2017.17	0.02000	0.015		CIRC	3.00	0.00			
182	KO					22					
183	ΚK	CV41									
184	RD	266.177	0.01280	0.015		CIRC	3.00	0.00			
185	KO					22					
186	ΚK	CV38									
187	RD	329.565	0.00750	0.015		CIRC	3.00	0.00			
188	KO					22					
189	ΚK	CV39									
190	RD	335.146	0.00460	0.015		CIRC	3.00	0.00			
191	KO					22					
192	ΚK	SB36									
193	BA	0.0435									
194	LS	0.1	98.000			68.287	0.1				
195	UK	2 5	.02	.1	20.24						
196	UK	60	.02	. 4	79.76						
197	RD	400	.01	.02	.005	TRAP	2	25			
198	RD	800	.015	.015		CIRC	1.5				
199	KO					22					
200	KK	HC18									
201	HC	2									
202	KO					22					
203	νv	CVAO									
204	RD	183.028	0.00460	0.015		CIRC	3.00	0.00			
205	KD KD	103.020	5.00400	0.010		22	5.00	0.00			
205	KŬ					22					
206	KK	DB5									
207	RS		FLOW								
208	SV	0	0.5	1	1.5	2	2.5	3			
209	SE	0	0.5	1	1.5	2	2.5	3			
210	SO	0	0.25	0.5	1	2	3	10			
211	КО					22					

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LINE	ID.	1.	2	3.	4.		б	7	. 8 9	10	
212	KK	SB34									
213	ВA	0.0271									
214	LS	0.1	98.000			69.482	0.1				
215	UK	20	.02	.1	4.63						
216	UK	100	.02	. 4	95.37						
217	RD	100	.025	.015		CIRC	1.25				
218	KO					22					
219	KK	SB33									
220	BA	0.0181									
221	LS	0.1	98.000			64.990	0.1				

222	UK	25	.02	.1	39.72					
223	UK	6 0	.02	. 4	60.28					
224	RD	300	.02	.02	.004	TRAP	2	2 5		
225	RD	1300	.02	.015		CIRC	1.25			
226	KO					22				
227	KK	HC13								
228	HC	2								
229	KO					22				
230	KK	CV21								
231	RD	764.982	0.02080	0.015		CIRC	2.00	0.00		
232	KO					22				
233	KK	SB35								
234	ВA	0.0295								
235	LS	0.1	98.000			74.938	0.1			
236	UK	2 5	.02	.1	20.58					
237	UK	60	.02	. 4	79.42					
238	RD	400	.02	.02	.004	TRAP	2	25		
239	RD	760	.02	.015		CIRC	1.25			
240	KO					22				
241	KK	HC14								
242	HC	2								
243	KO					22				
244	ΚK	CV22								
245	RD	202.938	0.00500	0.015		CIRC	2.00	0.00		
246	KO					22				
247	KK	DB4								
248	RS		FLOW							
249	SV	0	0.5	1	1.5	2	2.5	3	3.5	
250	SE	0	. 5	1	1.5	2	2.5	3	3.5	
251	SQ	0	0.25	0.5	1	2	4	5	15	
252	KO					22				

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253	ΚK	CV23							
254	RD	807.569	0.02000	0.040		TRAP	4.00	2.00	
255	KO					22			
256	КК	HC27							
257	HC	2							
258	ко					22			
259	КК	CV18							
260	RD	1608.00	0.02000	0.040		TRAP	4.00	2.00	
261	KO	2000.00	0.02000	0.010		22	1.00	2.00	
2.62	КК	CV100							
263	RD	1460 09	0 02000	0 040		TRAP	4 0 0	2 0 0	
264	KO	1100.00	0.02000	0.010		22	1.00	2.00	
201	110								
265	кк	SB113							
265		0 0748							
267	TC	0.0748	98 000			70 000	0 1		
207	10	25	50.000	1	25 00	/0.000	0.1		
200	UN	2.5	.02	. 1	25.00				
209	UN	400	.02	.4	/3.00		2	2 5	
270	KD	400	.01	.02		INAP	2	2.5	
211	KU					22			
272	VV	CV104							
272	nn DD	1071 00	0 01000	0 014		GIDG	2 0 0	0 0 0	
273	KD KO	10/1.00	0.01000	0.014		CIRC	2.00	0.00	
2/4	KU					22			
275	VV	0020							
275	LU LU	0 0705							
270	BA	0.0725	0.0 0.0 0			70 500	0 1		
277	12	0.1	98.000	1	25 00	/0.580	0.1		
278	UK	2.5	.02	. 1	25.00				
279	UK	1200	.02	.4	/5.00		2	0.5	
280	RD	1300	.01	.02	.06	TRAP	2	23	
281	RD	2700	.02	.04		TRAP	5	2	
282	KU					22			
202	77.77	00111							
203	KK D	0 0000							
∠ 8 4 2 8 5	BA	0.0990	0.0 0.0 0			70 000	0 1		
285	LS	0.1	98.000	1	05 00	/0.000	0.1		
280	UK	25	.02	• 1	25.00				
287	UK	60	.02	. 4	/5.00		-		
288	RD	1000	.01	.02	.05	TRAP	2	25	
289	RD	2000	.02	.015		CIRC	1.5		
290	KO					22			
291	KK	HC80							
292	HC	2				_			
293	KO					22			

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LINE ID.....1.....2.....3.....4.....5.....6......7.....8.....9.....10

294	KK	CV102									
295	RD	1300.49	0.02000	0.015		CIRC	2.50	0.00			
296	KO					22					
297	KK	SB112									
298	BA	0.0603									
299	LS	0.1	98.000			70.000	0.1				
300	UK	25	.02	.1	25.00						
301	UK	60	.02	. 4	75.00						
302	RD	1000	.01	.02	.05	TRAP	2	25			
303	RD	1000	.02	.015		CIRC	1.5				
304	KO					22					
305	ΚK	HC73									
306	HC	2									
307	KO					22					
308	ΚK	CV103									
309	RD	1133.61	0.02000	0.015		CIRC	3.00	0.00			
310	KO					22					
311	KK	HC79									
312	HC	2									
313	KO					22					
314	KK	DB10									
315	RS		F.TOM								
316	SV	0	.5	1	1.5	2	2.5	3	4	5	5.1
317	SE	0	.5	1	1.5	2	2.5	3	3.5	4	4.1
318	SQ	0	3	6	10	15	20	2 0	2 0	20	8 (
319	KO					22					
320	KK	HC12									
321	HC	3									
322	KO					22					
202	14.14	01101									
323	N.N.	1010 05		0 0 4 0			4 0 0	0 0 0			
324	RD	1812.85	0.02000	0.040		TRAP	4.00	2.00			
325	KO					22					
226	77.77	00110									
320	N.N.	SBIIU									
327	BA	0.0602				70 000	0 1				
328	LS	0.1	98.000			12.000	0.1				
329	UK	25	.02	. 1	25.00						
330	UK	60	.02	. 4	75.00						
331	RD	1000	.02	.015		CIRC	1.5				
332	KO					22					
2.2.2		H0D110			DOM DECT						
333	KK	USB110	DETENTION	BASIN F	ROM REGU	LATED AN	REAS				
334	KM	ELEVA	LION CURV	E IS VOL	UME IN A	C-FT OF	THEORETI	CAL DETE	NTION BA	ASIN	
335	RS		FLOW	0							
336	SV	0.0000	0.0542	0.1096	0.1639	0.2349	0.3072	0.3783	0.4385	0.4928	0.548
337	SE	0.0000	0.0542	0.1096	0.1639	0.2349	0.3072	0.3783	0.4385	0.4928	0.548
338	SQ	0.0000	3.1613	4.4335	5.4359	6.2841	7.0552	7.7106	8.0961	8.4816	23.13

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LINE	ID	1	2.	3.	4.	5.	6.	7.	8.	9.	10
339	КО					22					
340	КК	CV105									
341	RD	1143 83	0 00500	0 015		CIRC	1 7 5	0 0 0			
342	KO	1110.00	0.00000	0.010		22	1.70	0.00			
0.12	110										
343	КK	SB118									
344	BA	0.0544									
345	LS	0.1	89.000			72.000	0.1				
346	UK	25	.02	.1	25.00						
347	UK	60	.02	. 4	75.00						
348	RD	500	.01	.015		CIRC	1.5				
349	KO					22					
350	ΚK	USB118	DETENTION	I BASIN F	ROM REGU	LATED AF	REAS				
351	KM	ELEVA	TION CURV	'E IS VOL	UME IN A	C-FT OF	THEORETI	CAL DETE	NTION BA	SIN	
352	RS		FLOW	0							
353	SV	0.0000	0.0490	0.0991	0.1481	0.2123	0.2776	0.3419	0.3963	0.4453	0.495
354	SE	0.0000	0.0490	0.0991	0.1481	0.2123	0.2776	0.3419	0.3963	0.4453	0.495
355	SQ	0.0000	2.8570	4.0068	4.9127	5.6792	6.3760	6.9684	7.3168	7.6652	20.90
356	KO					22					
357	KK	HC71									
358	HC	3									
359	KO					22					
360	KK	CV20									
361	RD	2094.31	0.02000	0.040		TRAP	4.00	2.00			
362	KO					22					
363	KK	SB72									
364	BA	0.2119									
365	LS	0.1	98.000			71.870	0.1				
366	UK	25	.02	.1	25.00						
367	UK	60	.02	. 4	75.00						
368	RD	1000	.01	.02	.05	TRAP	2	25			
369	RD	3800	.02	.04		TRAP	5	2			
370	KO					22					
371	KK	USB72	DETENTION	I BASIN F	ROM REGU	LATED AF	REAS				
372	км	ELEVA	TION CURV	E IS VOL	UME IN A	C-FT OF	THEORETI	CAL DETE	NTTON BA	SIN	
373	RS		FLOW	01					211		
374	SV	0.0000	0.1907	0.3856	0.5764	0.8264	1.0806	1.3306	1.5425	1.7332	1.928
375	SF	0.0000	0.1907	0.3856	0.5764	0.8264	1.0806	1.3306	1.5425	1.7332	1.928
376	20 20	0 0000	11 120	15 595	19 121	22 104	24 817	27 122	28 478	29 834	81 36
377	кU 20	0.0000	11.120	-0.000	- /	22.104	27.01/	- / •	20.170	20.004	01.00
5,,,	10					~ ~ ~					
378	Кĸ	HC28									
379	HC	2									
380	KO	-				2.2					

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0.25 1.50 1

LINE ID.....1.....2......3.....4.....5......6......7......8......9.....10

381	ΚK	CV95								
382	RD	523.591	0.02000	0.040		TRAP	4.00	2.00		
383	KO					22				
384	КK	SB75								
385	BA	0.0498								
386	LS	0.1	98.000			75.410	0.1			
387	UK	25	.02	.1	75.00					
388	UK	60	.02	. 4	25.00					
389	RD	500	.02	.04	.005	TRAP	2	25		
390	RD	500	.02	.04		TRAP	2	2		
391	KO					22				
392	КK	CV88								
393	RD	1281.56	0.02000	0.015		CIRC	3.00	0.00		
394	KO					22				
395	КK	CV89								
396	RD	418.210	0.02000	0.015		CIRC	3.00	0.00		
397	KO					22				
398	КK	SB45								
399	BA	0.0163								
400	LS	0.1	98.000			73.593	0.1			
401	UK	25	.02	. 1	27.65					
402	UK	60	.02	. 4	72.35					
403	RD	900	.02	.02		TRAP	2	25		
404	ко					22				
405	KK	DB6								
406	RS		FLOW							
407	SV	0	0.025	0.05	0.075	0.1	0.125	0.15	0.2	0.225
408	SE	0	0.17	0.33	0.50	0.67	0.83	1.00	1.17	1.33
409	so	0	0	0	0	0	0	0	0.25	0.5
410	KO					22				
411	КК	SB29								
412	BA	0.0646								
413	LS	0.1	98.000			74.820	0.1			
414	11K 11C	25	02	1	25 00					
415	11K	2.5 6.0	.02	• ± 4	75 00					
416	0 N D N	400	.02	. 4	, 5.00	TRAP	2	2.5		
417	תת חק	1000	.02	.02	.01	TRAP	2	2 2		
119	KO KO	1000	.01	.04		20	2	4		
4 1 0	NU					22				
410	17.17	1070								
120	NA HC	лс/8 э								
4∠U 4.2.1	HC	Z				2.2				
4 2 1	KO					22				

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9.1 4.5 50

422	KK	CV91								
423	RD	1587.23	0.00500	0.015		CIRC	2.50	0.00		
424	KO					22				
425	ΚK	SB73								
426	BA	0.1674								
427	LS	0.1	98.000			73.350	0.1			
428	UK	2 5	.02	.1	25.00					
429	UK	60	.02	. 4	75.00					
430	RD	400	.02	.02	.01	TRAP	2	25		
431	RD	1000	.01	.04		TRAP	2	2		
432	KO					22				
4.2.2										
433	KK	HC63								
434	HC	3								
435	KO					22				
136	ĸĸ	CVAO								
430	RIC	1552 93	0 02000	0 014		CIRC	3 5 0	0 00		
439	KO	1332.93	0.02000	0.014		22	5.50	0.00		
450	110					22				
439	КK	SB103								
440	BA	0.0685								
441	LS	0.1	98.000			75.000	0.1			
442	UK	25	.02	. 1	25.00					
443	UK	60	.02	. 4	75.00					
444	RD	250	.01	.02	.01	TRAP	2	25		
445	RD	500	.01	.015		CIRC	2			
446	KO					22				
447	KK	H C 6 4								
448	HC	2								
449	KO					22				
450	KK	DB13								
451	RS		FLOW							
452	SV	0	1	2	3	5	6	7	8	9
453	SE	0	1	1.5	2	2.5	3	3.5	4	4.25
454	SQ	0	3	6	12	20	2 5	26	27	27.5
455	KO					22				
156	VV	CVEO								
457	RD	2456 98	0 00600	0 015		CIRC	2 50	0 0 0		
458	KO	2400.00	0.00000	0.015		22	2.00	0.00		
	110									
459	KK	SB99								
460	BA	0.0809								
461	LS	0.1	98.000			77.000	0.1			
462	UK	25	.02	.1	25.00					
463	UK	60	.02	. 4	75.00					
464	RD	400	.005	.015		CIRC	1.5			
465	KO					22				

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LINE	ID	1	2.	3.	4.	5.	6.	7.	8.	9.	10
1.5.5											
466	KK	USB991	DETENTION	I BASIN F	NOM REGU	CATED AF	(EAS		NETON DA	C T N	
467	KM	ELEVA	FION CURV	'E IS VOI	UME IN A	C-FT OF	THEORETI	CAL DETE	NTION BA	SIN	
468	RS		FLOW	0							0.000
469	SV	0.0000	0.0728	0.14/3	0.2201	0.3156	0.4127	0.5082	0.5891	0.6619	0.736
4 / 0	SE	0.0000	0.0728	0.14/3	0.2201	0.3156	0.4127	0.5082	0.5891	0.6619	0./36
4/1	SQ	0.0000	4.246/	5.955/	1.3022	8.4416	9.4//3	10.357	10.8/5	11.393	31.07
4 / 2	KO					22					
172	VV	11067									
473	N.C.	1007									
474	нс	5				2.2					
475	KU					22					
176	ĸĸ	0175.2									
470	RD	1503 11	0 02000	0 040		TRAP	4 0 0	2 0 0			
477	KO	1303.11	0.02000	0.040		22	4.00	2.00			
470	KU					22					
479	кк	CBOS									
480	BA	0 0373									
481	LS	0.09,9	98 000			86 000	0 1				
482	IIK	5.0	02	1.4	60 00	00.000	0.1				
483	11K	30	.02	. 1 4	40.00						
484	BD.	1300	0.2	015	10.00	CIRC	2				
485	KO	1000	.02	.010		22	-				
486	KK	USB931	DETENTION	BASIN F	ROM REGU	LATED AF	REAS				
487	КM	ELEVA	TION CURV	'E IS VOI	UME IN A	C-FT OF	THEORETI	CAL DETE	NTION BA	SIN	
488	RS		FLOW	0							
489	SV	0.0000	0.0806	0.1629	0.2435	0.3491	0.4565	0.5622	0.6517	0.7322	0.814
490	SE	0.0000	0.0806	0.1629	0.2435	0.3491	0.4565	0.5622	0.6517	0.7322	0.814
491	SQ	0.0000	1.9574	2.7451	3.3658	3.8909	4.3683	4.7742	5.0129	5.2516	14.32
492	KO					22					
493	КK	CV93									
494	RD	600.955	0.01000	0.015		CIRC	1.50	0.00			
495	KO					22					
496	KK	SB94									
497	BA	0.0409									
498	LS	0.1	98.000			86.000	0.1				
499	UK	50	.02	.14	60.00						
500	UK	30	.02	. 4	40.00						
501	RD	1300	.02	.015		CIRC	2				
502	KO					22					
503	KK	USB941	DETENTION	BASIN F	ROM REGU	LATED AF	REAS				
504	КM	ELEVA	TION CURV	'E IS VOI	UME IN A	C-FT OF	THEORETI	CAL DETE	NTION BA	SIN	
505	RS		FLOW	0							
506	SV	0.0000	0.0884	0.1788	0.2673	0.3832	0.5011	0.6170	0.7153	0.8037	0.894
507	SE	0.0000	0.0884	0.1788	0.2673	0.3832	0.5011	0.6170	0.7153	0.8037	0.894
508	SQ	0.0000	2.1484	3.0131	3.6943	4.2707	4.7947	5.2402	5.5022	5.7642	15.72
509	KO					22					

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LINE ID.....1.....2......3......4......5......6......7.....8......9.....10 510 ΚK HC65 НC 2 511 512 KO 22 513 KK CV94 514 RD 623.598 0.01000 0.015 CIRC 2.00 0.00 515 KO 22 516 ΚK HC51 517 HC 2 518 22 KO 519 KK CV71 520 RD 1198.25 0.02000 0.040 TRAP 4.00 2.00 521 KO 22 522 KK SB98 BA 0.0538 523 524 LS 0.1 98.000 86.000 0.1 50 .02 .1 40.00 525 UK .02 526 UK 30 .4 60.00 .015 527 RD 1000 .02 CIRC 1.5 KO 22 528 KK USB98DETENTION BASIN FROM REGULATED AREAS 529 KM ELEVATION CURVE IS VOLUME IN AC-FT OF THEORETICAL DETENTION BASIN 530 0 531 RS FLOW 532 SV 0.0000 0.0774 0.1565 0.2339 0.3354 0.4386 0.5401 0.6261 0.7035 0.782 533 SE 0.0000 0.0774 0.1565 0.2339 0.3354 0.4386 0.5401 0.6261 0.7035 0.782 534 SQ 0.0000 2.8209 3.9562 4.8506 5.6075 6.2955 6.8804 7.2244 7.5684 20.64 535 KO 22 536 КK SB49 BA 0.0380 537 0.1 98.000 75.038 538 LS 0.1 .1 15.00 .02 539 UK 25 540 UK 90 .02 .4 85.00 541 RD 500 .02 .02 .01 TRAP 2 25 542 RD 500 .02 .04 TRAP 1 2 543 KO 22 KK USB49DETENTION BASIN FROM REGULATED AREAS 544 KM ELEVATION CURVE IS VOLUME IN AC-FT OF THEORETICAL DETENTION BASIN 545 FLOW 0 546 RS SV 0.0000 0.0205 0.0415 0.0620 0.0889 0.1162 0.1431 0.1659 0.1864 0.207 547 SE 0.0000 0.0205 0.0415 0.0620 0.0889 0.1162 0.1431 0.1659 0.1864 0.207 548 SQ 0.0000 1.9931 2.7953 3.4272 3.9620 4.4481 4.8614 5.1044 5.3475 14.58 549 550 KO 22

ID.....1.....2......3.....4.....5......6......7......8......9.....10

551 KK CV24 RD 962.679 0.00500 0.015 552 CIRC 1.50 0.00 553 KO 22 554 ΚK SB48 555 BA 0.0374 556 LS 0.1 98.000 73.160 0.1 557 UK 25 .02 .1 15.00 558 UK 90 .02 .4 85.00 559 RD 600 .02 .02 .005 TRAP 2 25 560 RD 800 .02 .04 TRAP 2 2 561 KO 22 562 KK USB48DETENTION BASIN FROM REGULATED AREAS 563 КM ELEVATION CURVE IS VOLUME IN AC-FT OF THEORETICAL DETENTION BASIN RS FLOW 0 564 565 SV 0.0000 0.0202 0.0408 0.0610 0.0874 0.1143 0.1408 0.1632 0.1834 0.204 SE 0.0000 0.0202 0.0408 0.0610 0.0874 0.1143 0.1408 0.1632 0.1834 0.204 566 SQ 0.0000 1.9606 2.7496 3.3713 3.8973 4.3755 4.782 5.0211 5.2602 14.346 567 568 KO 22 569 ΚK HC55 570 HC 2 571 KO 22 572 KK CV64 573 RD 1426.23 0.01800 0.015 CIRC 1.50 2.00 574 KO 22 575 KK SB117 576 BA 0.0456 577 0.1 98.000 LS 72.000 0.1 .1 25.00 578 UK 25 .02 579 60 .02 .4 75.00 UK 580 800 .023 RD .005 .015 CIRC 1.5 581 RD 300 .01 .02 CIRC 1.5 582 KO 22 583 KK USB117DETENTION BASIN FROM REGULATED AREAS 584 KM ELEVATION CURVE IS VOLUME IN AC-FT OF THEORETICAL DETENTION BASIN 585 RS FLOW 0 586 SV 0.0000 0.0411 0.0831 0.1241 0.1780 0.2327 0.2866 0.3322 0.3733 0.415 587 SE 0.0000 0.0411 0.0831 0.1241 0.1780 0.2327 0.2866 0.3322 0.3733 0.415 SQ 0.0000 2.3948 3.3585 4.1179 4.7604 5.3445 5.841 6.1330 6.4251 17.523 588 KO 22 589 КK SB88 590 BA 0.0337 591 0.1 98.000 592 LS 77.000 0 1 25 .1 25.00 593 UK .02 60 .02 594 UK .4 75.00 RD 400 .005 .015 CIRC 595 1.5 596 KO 22

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LINE	ID.	1	2.		4.	5	6.	7.	8.	9.	10
597	ΚK	USB881	DETENTION	I BASIN F	FROM REGU	LATED AF	REAS				
598	КМ	ELEVA	FION CURV	VE IS VOI	LUME IN A	C-FT OF	THEORETI	CAL DETE	NTION BA	SIN	
599	RS		FLOW	0							
600	SV	0.0000	0.0303	0.0614	0.0917	0.1315	0.1720	0.2118	0.2455	0.2758	0.306
601	SE	0.0000	0.0303	0.0614	0.0917	0.1315	0.1720	0.2118	0.2455	0.2758	0.306
602	SQ	0.0000	1.7696	2.4818	3.0429	3.5177	3.9493	4.3162	4.5320	4.7478	12.94
603	KO					22					
604	17.17	11000									
604	K K	HCZ3									
605	HC	2				2.2					
000	RO					22					
607	КК	CV114									
608	RD	1318.87	0.01000	0.014		CIRC	1.50	0.00			
609	ко					22					
610	КK	SB91									
611	ВA	0.0589									
612	LS	0.1	98.000			86.000	0.1				
613	UK	50	.02	.14	60.00						
614	UK	30	.02	. 4	40.00						
615	RD	1300	.02	.015		CIRC	2				
616	KO					22					
617	KK	USB911	DETENTION	I BASIN F	FROM REGU	LATED AN	REAS				
618	KM	ELEVA	FION CURV	E IS VOI	JUME IN A	C-FT OF	THEORETI	CAL DETE	INTION BA	SIN	
619	RS		FLOW	0							1 000
620	SV	0.0000	0.1272	0.2572	0.3845	0.5512	0.7209	0.8876	1.0289	1.1562	1.286
621	SE	0.0000	0.1272	1 22/5	0.3843	6 1 4 2 0	6 9076	7 5 2 0 / 0	1.0209 7.0152	0 2022	1.200
623	2Q	0.0000	3.0907	4.3343	J.J14J	0.1430	0.09/0	1.3304	1.9133	0.2922	22.01
025	110					22					
624	KK	SB89									
625	BA	0.0438									
626	LS	0.1	98.000			86.000	0.1				
627	UK	50	.02	.14	60.00						
628	UK	30	.02	. 4	40.00						
629	RD	500	.005	.015		CIRC	2				
630	KO					22					
631	ΚK	USB891	DETENTION	N BASIN F	FROM REGU	LATED AF	REAS				
632	KM	ELEVA	FION CURV	VE IS VOI	LUME IN A	C-FT OF	THEORETI	CAL DETE	NTION BA	SIN	
633	RS		FLOW	0							
634	SV	0.0000	0.0947	0.1915	0.2862	0.4103	0.5365	0.6607	0.7659	0.8606	0.957
635	SE	0.0000	0.0947	0.1915	0.2862	0.4103	0.5365	0.6607	0.7659	0.8606	0.957
636	SQ	0.0000	2.3004	3.2262	3.9556	4.5728	5.1338	5.6108	5.8913	6.1718	16.83
637	KO					22					
620	12.12	UCAE									
030	KK	нс45									
640	RO RO	4				2.2					
0 1 0	1.0					~ ~ ~					

LINE ID.....1.....2......3.....4.....5......6......7......8......9.....10 641 KK CV65 RD 977.717 0.01800 0.015 642 CIRC 2.50 2.00 22 643 KO 644 KK SB107 645 BA 0.0224 646 LS 0.1 98.000 77.000 0.1 .1 25.00 647 UK 25 .02 648 UK 60 .02 .4 75.00 649 RD 500 .02 .015 CIRC 1.5 650 KO 22 651 KK USB107DETENTION BASIN FROM REGULATED AREAS 652 KM ELEVATION CURVE IS VOLUME IN AC-FT OF THEORETICAL DETENTION BASIN 653 RS FLOW 0 SV 0.0000 0.0202 0.0408 0.0609 0.0874 0.1143 0.1407 0.1631 0.1833 0.203 654 655 SE 0.0000 0.0202 0.0408 0.0609 0.0874 0.1143 0.1407 0.1631 0.1833 0.203 SQ 0.0000 1.1757 1.6488 2.0216 2.3370 2.6238 2.8676 3.0109 3.1543 8.602 656 KO 657 22 658 KK CV97 659 RD 996.647 0.00500 0.015 CIRC 2.00 0.00 660 KO 22 661 KK CV98 662 RD 563.543 0.00500 0.015 CIRC 1.50 0.00 663 KO 22 664 ΚK HC68 665 2 HC 666 KO 22 KK CV99 667 668 RD 566.379 0.02000 0.015 CIRC 2.50 0.00 669 KO 2.2 670 ΚK SB90 671 BA 0.0501 0.1 98.000 672 LS 86.000 0.1 .14 60.00 673 UK 50 .02 674 UK 30 .02 .4 40.00 1000 675 RD .01 .015 CIRC 2 676 KO 22 KK USB90DETENTION BASIN FROM REGULATED AREAS 677 678 KM ELEVATION CURVE IS VOLUME IN AC-FT OF THEORETICAL DETENTION BASIN 679 RS FLOW 0 SV 0.0000 0.1083 0.2190 0.3273 0.4694 0.6138 0.7558 0.8761 0.9845 1.095 680 SE 0.0000 0.1083 0.2190 0.3273 0.4694 0.6138 0.7558 0.8761 0.9845 1.095 681 682 SQ 0.0000 2.6316 3.6907 4.5251 5.2311 5.8730 6.4186 6.7395 7.0604 19.25 683 ко 22

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684 KK CV66 RD 740.469 0.00500 0.015 685 CIRC 2.50 0.00 686 KO 22 687 ΚK HC46 688 HC 2 689 KO 22 690 KK CV67 691 RD 457.366 0.00400 0.014 CIRC 3.50 0.00 692 KO 22 693 KK SB92 694 BA 0.0396 695 LS 0.1 98.000 86.000 0.1 50 .02 696 UK .1 60.00 .02 697 UK 30 .4 40.00 .02 698 RD 1000 .015 CIRC 2 699 KO 22 KK USB92DETENTION BASIN FROM REGULATED AREAS 700 701 KM ELEVATION CURVE IS VOLUME IN AC-FT OF THEORETICAL DETENTION BASIN 702 RS FLOW 0 SV 0.0000 0.0855 0.1729 0.2584 0.3705 0.4845 0.5966 0.6916 0.7771 0.864 703 704 SE 0.0000 0.0855 0.1729 0.2584 0.3705 0.4845 0.5966 0.6916 0.7771 0.864 705 sq 0.0000 2.0773 2.9133 3.5719 4.1292 4.6359 5.0666 5.3199 5.5732 15.19 706 KO 22 707 KK SB104 708 BA 0.0264 709 LS 0.1 98.000 86.000 0.1 .1 60.00 50 710 UK .02 30 711 .02 .4 40.00 UK 500 712 .02 RD .015 CIRC 1.5 713 KO 22 714 KK USB104DETENTION BASIN FROM REGULATED AREAS 715 KM ELEVATION CURVE IS VOLUME IN AC-FT OF THEORETICAL DETENTION BASIN 716 RS FLOW 0 SV 0.0000 0.0570 0.1153 0.1723 0.2470 0.3230 0.3977 0.4611 0.5181 0.576 717 718 SE 0.0000 0.0570 0.1153 0.1723 0.2470 0.3230 0.3977 0.4611 0.5181 0.576 719 SQ 0.0000 1.3849 1.9422 2.3813 2.7529 3.0906 3.3778 3.5466 3.7155 10.13 720 KO 22 КK HC47 721 722 HC 3 723 KO 22 724 KK CV68 725 RD 887.251 0.00500 0.014 CIRC 3.50 0.00 726 ко 22

LINE ID.....1.....2......3.....4.....5......6......7......8......9.....10 727 KK SB105 728 BA 0.0163 729 0.1 98.000 86.000 LS 0.1 .1 60.00 730 UK 25 .02 731 UK 30 .02 .4 40.00 732 RD 500 .02 .015 CIRC 1.5 733 KO 22 734 KK USB105DETENTION BASIN FROM REGULATED AREAS 735 KM ELEVATION CURVE IS VOLUME IN AC-FT OF THEORETICAL DETENTION BASIN 736 FLOW 0 RS 737 SV 0.0000 0.0352 0.0712 0.1063 0.1525 0.1994 0.2455 0.2846 0.3198 0.355 738 SE 0.0000 0.0352 0.0712 0.1063 0.1525 0.1994 0.2455 0.2846 0.3198 0.355 739 SQ 0.0000 0.8549 1.1989 1.4700 1.6994 1.9079 2.0852 2.1894 2.2937 6.255 740 KO 22 741 ΚK HC48 742 HC 2 KO 743 22 744 KK CV69 745 RD 469.429 0.00500 0.014 CIRC 3.50 0.00 746 KO 22 747 KK SB106 748 BA 0.0228 749 LS 0.1 98.000 86.000 0.1 .1 40.00 750 UK 50 .02 751 UK 30 .02 .4 60.00 752 RD 300 .02 .015 CIRC 1.5 753 KO 22 KK USB106DETENTION BASIN FROM REGULATED AREAS 754 755 KM ELEVATION CURVE IS VOLUME IN AC-FT OF THEORETICAL DETENTION BASIN 756 FLOW RS 0 757 SV 0.0000 0.0328 0.0663 0.0991 0.1422 0.1859 0.2289 0.2654 0.2982 0.331 SE 0.0000 0.0328 0.0663 0.0991 0.1422 0.1859 0.2289 0.2654 0.2982 0.331 758 SQ 0.0000 1.1955 1.6767 2.0557 2.3765 2.6681 2.916 3.0618 3.2076 8.748 759 22 760 KO 761 ΚK HC49 762 НC 2 763 KO 22 КK CV70 764 765 RD 1368.21 0.00400 0.014 CIRC 4.00 0.00 766 KO 22 767 КK HC50 768 HC 2 769 KO 22

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#### HEC-1 INPUT

## LINE ID.....1......2......3......4.....5.....6......7......8......9.....10

770 K	K CV78						
771 F	D 498.057	0.02000	0.040		TRAP	4.00	2.00
772 к	0				22		
773 к	K SB40						
774 P	A 0 0401						
775 T	s 0 1	98 000			73 232	0 1	
776 1	к 25	0.2	1	28 00			
777 1	к 60	0.2		72 00			
778 5	n 900	01	0.4	008	TRAP	2	25
779 F	D 1000	02	015	.000	CIRC	1 2 5	20
780 K	0	.02	.010		22	1.20	
	0						
781 к	K DB7						
782 5	s	FLOW					
783 9	V 0	1 1	2	3			
784 9	E 0	- 5	- 1	15			
785 8	0 0	2	- 8	12			
786 K	0	-	0		22		
	0						
787 к	K CV25						
788 F	D 481.517	0.03830	0.015		CIRC	1.50	0.00
789 K	0				22		
790 к	к ѕвзэ						
791 E	A 0.0230						
792 I	s 0.1	98.000			75.333	0.1	
793 U	к 25	.02	. 1	34.79			
794 U	к 60	.02	. 4	65.21			
795 F	D 400	.02	.04	.005	TRAP	2	25
796 F	D 975	.01	.015		CIRC	1.25	2
797 к	0				22		
798 к	K SB41						
799 E	A 0.0172						
800 I	s 0.1	98.000			75.456	0.1	
801 U	к 30	.01	.1	42.90			
802 U	к 50	.02	. 4	57.10			
803 F	D 500	.01	.04		TRAP	2	25
804 K	0				22		
805 K	к нсзі						
806 H	с з						
807 K	0				22		
808 K	K CV26						
809 F	D 1005.34	0.00750	0.014		CIRC	2.00	0.00
810 K	0				22		

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LINE	ID1	2	.3	.4	.5	. 6	. 7	. 8	.9	.10

811	ΚK	SB37							
812	BA	0.0248							
813	LS	0.1	98.000			76.000	0.1		
814	UK	25	.02	.1	25.00				
815	UK	60	.02	. 4	75.00				
816	RD.	400	0.1	0.4	0.05	TRAP	2	25	
817	RD	500	.01	015	.000	CIRC	1 2 5	20	
818	KO	500	.02	.015		22	1.20		
010	10					22			
810	νv	CVES							
820	NN NN	733 376	0 02760	0 015		CIPC	1 50	0 0 0	
020	RD	133.320	0.02760	0.015		CIRC	1.50	0.00	
021	KU					22			
0.0.0		0.5.2.0							
822	KK	SB38							
823	BA	0.0182							
824	LS	0.1	98.000			75.606	0.1		
825	UK	30	.01	.1	36.48				
826	UK	50	.02	. 4	63.52				
827	RD	300	.01	.02	.005	TRAP	2	25	
828	RD	500	.01	.015		CIRC	1.25		
829	KO					22			
830	ΚK	HC35							
831	HC	2							
832	KO					22			
833	KK	CV27							
8.3.4	RD	1238.85	0.00660	0.014		CIRC	2.00	0.00	
835	K O					22			
000	110								
836	КК	SB43							
837	RA	0 0262							
030	DA	0.0202	00 000			70 500	0 1		
030	112	25	50.000	1	14 46	/0.500	0.1		
039	UK	2.5	.02	• 1	14.40				
040	UK	60	.02	. 4	83.34		2	0 F	
041	RD	400	.01	. U Z		TRAP	Z	2 5	
04∠	KO					22			
0.4.2									
843	KK	нсз2							
844	HC	3				_			
845	KO					22			
846	ΚK	CV28							
847	RD	630.174	0.02880	0.015		CIRC	2.50	0.00	
848	KO					22			
849	ΚK	SB44							
850	BA	0.0344							
851	LS	0.1	98.000			70.014	0.1		
852	UK	25	.02	.1	22.83				
853	UK	60	.02	. 4	77.17				
854	RD	400	.01	.02	.005	TRAP	2	25	
855	RD	830	. 0 1	.015		CIRC	1.25	-	
856	KO	000		.010		22	1.20		
000	I(U)					~ ~			

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#### HEC-1 INPUT

## LINE ID.....1.....2......3.....4.....5.....6......7......8.....9.....10

957	ĸĸ	4036									
857	NA NA	псэо									
050	пс	2				2.2					
839	KÜ					22					
0.00		G110 0									
860	KK	0.029		0 015			0 5 0	0 0 0			
861	RD	345.220	0.02880	0.015		CIRC	2.50	0.00			
862	KO					22					
0.60											
863	K.K.	SB46									
864	BA	0.0120									
865	LS	0.1	98.000			/6.000	0.1				
866	UK	25	.02	.1	25.00						
867	UK	60	.02	. 4	/5.00						
868	RD	800	.01	.04		TRAP	2	25			
869	KO					22					
870	ΚK	HC33									
871	HC	2									
872	KO					22					
873	ΚK	CV30									
874	RD	185.232	0.00500	0.015		CIRC	2.50	0.00			
875	KO					22					
876	ΚK	SB42									
877	BA	0.0770									
878	LS	0.1	98.000			71.325	0.1				
879	UK	50	.02	.1	0.10						
880	UK	200	.02	. 4	99.90						
881	RD	1400	.02	.015		CIRC	2				
882	KO					22					
883	ΚK	HC34									
884	HC	2									
885	KO					22					
886	ΚK	DB8									
887	RS		FLOW								
888	SV	0	1	2	3	4	5	6	7	8	
889	SE	0	0.33	0.67	1	1.33	1.67	2	2.33	2.67	
890	SQ	0	0	1	2	4	8	16	25	25	
891	KO					22					
892	KK	CV119									
893	RD	1473.36	0.00500	0.015		CIRC	2.00	0.00			
894	KO					22					
895	KK	SB76									
896	BA	0.0412									
897	LS	0.1	98.000			77.709	0.1				
898	UK	25	.02	.1	25.00						
899	UK	8 0	.02	. 4	75.00						
900	RD	1500	.02	.02	.005	TRAP	2	25			
901	RD	200	.02	.015		CIRC	1.5	2			
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HEC-1 INPUT
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LINE	тр	1	2	з	4	5	6	7	8	9	1.0
11111	10							•••••		••••••	
902	KO					22					
903	КК	SB47									
904	D 7	0 0469									
0.05	DA	0.0405	00 000			70 025	0 1				
905	12	25	50.000	1	15 00	19.933	0.1				
900	UK	2.5	.02	• 1	15.00						
907	NU DD	50	.02	• 4	03.00		2	0.5			
908	RD	500	.02	.02	.01	TRAP	2	25			
909	RD	500	.02	.04		IRAP	2	2			
910	KU					22					
911	KK	USB47	DETENTION	BASIN F	ROM REGU	LATED AF	REAS				
912	КМ	ELEVA	TION CURV	'E IS VOI	UME IN A	C-FT OF	THEORETI	CAL DETE	NTION BA	SIN	
913	RS		FLOW	0							
914	SV	0.0000	0.0253	0.0512	0.0765	0.1097	0.1434	0.1766	0.2047	0.2300	0.255
915	SE	0.0000	0.0253	0.0512	0.0765	0.1097	0.1434	0.1766	0.2047	0.2300	0.255
916	so	0.0000	2.4598	3.4497	4.2297	4.8896	5.4896	5.9996	6.2995	6.5995	17.99
917	KO					22					
918	KK	HC37									
919	HC	3									
920	KO					22					
921	ΚK	CV55	Proposed	pipe							
922	RD	1417.65	0.02000	0.015		CIRC	2.00	0.00			
923	KO					22					
924	KK	SB84									
925	BA	0.0375									
926	LS	0.1	98.000			77.000	0.1				
927	UK	25	.02	.1	25.00						
928	UK	60	.02	. 4	75.00						
929	RD	1300	.02	.015		CIRC	2				
930	KO					22					
931	кк	USB84	DETENTION	BASIN F	BOM RECH	ILATED AR	EAS				
932	KW VU	FLEVA	TTON CUPU	F TS VOT	.UMF TN A	C-FT OF	 	CAL DETE	NTION PA	SIN	
933	D C	E D E V A	FLOW	U 10 VOI	OTE IN A	IC FI OF	11501511	CUT DELE	NIION DA	U 1 IN	
934	21/	0 0000	0 0337	0 0682	0 1019	0 1462	0 1 9 1 1	0 2353	0 2728	0 3065	0 3/11
935	SF	0.0000	0.0337	0.0682	0 1019	0 1462	0 1911	0.2353	0 2728	0.3065	0.341
936	50	0.0000	1 9666	2 7581	3 3817	3 9093	4 3890	4 7968	5 0366	5 2764	14 39
937	KO SÕ	0.0000	1.9000	2.7501	5.5017	22	4.5050	4.7500	5.0500	5.2704	14.00
938	КK	HC20									
939	HC	2									
940	KO					22					
941	KK	CV79									
942	RD	1626.81	0.01940	0.014		CIRC	2.00	0.00			
943	KO					22					

ID.....1.....2......3.....4.....5......6......7......8......9.....10

944 KK CV61 945 RD 1181.90 0.00850 0.014 CIRC 2.50 0.00 946 KO 22 947 SB82 ΚK 948 BA 0.0425 949 LS 0.1 98.000 82.000 0.1 .1 60.00 950 UK 50 .02 951 UK 40 .02 .4 40.00 952 RD 1300 .02 .015 CIRC 1.5 953 KO 22 954 KK USB82DETENTION BASIN FROM REGULATED AREAS 955 КM ELEVATION CURVE IS VOLUME IN AC-FT OF THEORETICAL DETENTION BASIN 956 RS FLOW 0 957 SV 0.0000 0.0918 0.1855 0.2773 0.3976 0.5199 0.6402 0.7422 0.8339 0.927 958 SE 0.0000 0.0918 0.1855 0.2773 0.3976 0.5199 0.6402 0.7422 0.8339 0.927 SQ 0.0000 2.2292 3.1263 3.8332 4.4313 4.9750 5.4372 5.7090 5.9809 16.31 959 960 KO 22 961 ΚK HC82 962 HC 2 963 KO 22 KK CV84 964 965 RD 1169.01 0.00680 0.015 CIRC 2.50 0.00 966 KO 22 967 КK SB81 968 BA 0.0480 969 LS 0.1 98.000 77.000 0.1 .1 25.00 970 25 .02 UK 60 971 UK .02 .4 75.00 1300 972 .02 .015 CIRC 1.5 RD 973 22 KO 974 KK CV59 RD 590.170 0.00500 0.015 975 CIRC 2.25 0.00 976 22 KO 977 КK SB78 978 BA 0.0582 979 LS 0.1 98.000 77.000 0.1 980 UK 25 .02 .1 25.00 981 UK 60 .02 .4 75.00 982 RD 800 .01 .015 0.018 TRAP 1.5 RD 800 .02 .015 CIRC 983 1.5 KO 984 22

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LINE

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985	KK	CV86									
986	RD	1046.19	0.00500	0.015		CIRC	2.50	0.00			
987	KO					22					
988	КK	SB80									
989	BA	0.0454									
990	LS	0.1	98.000			77.000	0.1				
991	UK	25	.02	.1	25.00						
992	UK	6.0	. 0.2	. 4	75.00						
993	RD	1300	0.2	015		CIRC	15				
994	KO	1000	.02	.010		22	1.0				
554	100					22					
0.0 5	VV	11060									
995	NR UC	11000									
990	пс	5									
997	KO					22					
998	KK	DB15									
999	RS		FLOW								
1000	SV	0	.3	.6	. 9	1.2	1.5	1.8	2	2.1	2.2
1001	SE	0	.3	.6	.9	1.2	1.5	1.8	2	2.1	2.2
1002	SQ	0	2	5	10	14	16	18	20	25	50
1003	KO					22					
1004	KK	CV85									
1005	RD	196.193	0.00750	0.014		CIRC	2.00	0.00			
1006	KO					22					
1007	KK	HC43									
1008	HC	2									
1009	КО					22					
1010	KK	CV58									
1011	RD	1338.03	0.00250	0.014		CIRC	3.50	0.00			
1012	КО					22					
1013	кк	SB116									
1014	BA	0 0135									
1015	LS	0.0100	98 000			77 000	0 1				
1015	112	25	02	1	25 00	//.000	0.1				
1010	UK	2.5	.02	• 1	25.00						
1017	UK	60	.02	.4	/5.00						
1018	RD	/50	.02	.02		TRAP	2	25			
1019	KO					22					
1020	KK	HC41									
1021	HC	2									
1022	KO					22					
1023	ΚK	CV57									
1024	RD	507.761	0.00250	0.014		CIRC	3.50	0.00			
1025	KO					2.2					

LINE	ID	1	2.	3.	4.		6.	7.	8.	9.	10
1026	КK	SB115									
1027	ΒA	0.0301									
1028	LS	0.1	98.000			77.000	0.1				
1029	UK	25	.02	.1	40.00						
1030	UK	60	.02	. 4	60.00						
1031	RD	400	.02	.02		TRAP	2	25			
1032	KO					22					
1033	ĸĸ	IISB115	DETENTION	I BASIN F	ROM REGU		FAS				
1034	КМ	ELEVA	TION CURV	VE IS VOL	IIME IN A	C-FT OF	THEORETI	CAL DETE	NTION BA	SIN	
1035	RS		FLOW	1 10 101		.0 11 01	INDORUTI	CIIL DEIL	NIION DI	10111	
1036	SV	0 0000	0 0433	0 0875	0 1308	0 1876	0 2453	0 3020	0 3501	0 3934	0 437
1037	SF	0.0000	0.0433	0 0875	0 1308	0 1876	0 2453	0 3020	0.3501	0.3934	0.437
1038	80	0.0000	1 5774	2 2122	2 7124	3 1356	3 5203	3 8474	4 0397	4 2321	11 54
1020	20	0.0000	1.5774	2.2122	2.7124	3.1330	5.5205	5.04/4	4.0357	4.2321	11.34
1039	ĸŬ					22					
1040	КK	CV109									
1041	RD	1206.67	0.00300	0.015		CIRC	1.50	0.00			
1042	КO					22					
1042	VV	11 C Q 1									
1043	N.C.	ncoi									
1044	rc vo	2				2.2					
1045	кO					22					
1046	КK	CV117									
1047	RD	284.559	0.00230	0.014		CIRC	3.50	0.00			
1048	KO					22					
1049	ΚK	SB6									
1050	ΒA	0.0139									
1051	LS	0.1	98.000			75.000	0.1				
1052	UK	25	.02	.1	25.00						
1053	UK	60	.02	. 4	75.00						
1054	RD	700	.004	.02		TRAP	2	25			
1055	KO					22					
1056	КК	CV5									
1057	RD	504.839	0.00400	0.015		CIRC	1.25	0.00			
1058	KO					22					
1050	12.14										
1009	KK	CV6	0 00400	0 015		0.7.0.0	1 50	0 00			
1060	K D	850.434	0.00400	0.015		22	1.50	0.00			
TOOT	щU					22					
1062	ΚK	SB2									
1063	ΒA	0.0318									
1064	LS	0.1	98.000			79.826	0.1				
1065	UK	2 5	.02	.1	25.94						
1066	UK	60	.02	. 4	74.06						
1067	RD	350	.004	.02	.004	TRAP	2	25			
1068	RD	1330	.004	.015		CIRC	1.5				
1069	KO					22					

1070	КK	SB1						
1071	BA	0.0200						
1072	LS	0.1	98.000			79.698	0.1	
1073	UK	20	.02	.1	24.42			
1074	UK	60	.02	. 4	75.58			
1075	RD	850	. 0 0 4	.015		CIRC	1.5	
1076	RD	400	004	0.2	007	TRAP	2	25
1077	KO	100		.02		22	-	20
1077	110							
1078	КК	HC1						
1079	нс	3						
1080	ко	5				2.2		
1000	110							
1081	КК	CV1						
1002		270 025	0 00500	0 015		CIDC	2 0 0	0 0 0
1002	KD KO	570.055	0.00500	0.015		22	2.00	0.00
1002	KU					22		
1094	VV	002						
1095		0 0222						
1005	DA	0.0222	0.0 0.0 0			7.6 0.61	0 1	
1000	12	0.1	98.000	1	5 36	/0.001	0.1	
1087	UK	25	.02	• 1	5.30			
1088	UK	60	.02	. 4	94.64		0	0.5
1089	RD	/00	.004	.02	.0048	TRAP	2	25
1090	RD	400	.005	.015		CIRC	Z	
1091	KO					22		
1000								
1092	K.K.	HC4						
1093	HC	2						
1094	KO					22		
4.0.05								
1095	K K	CV2						
1096	RD	122.150	0.00500	0.015		CIRC	2.00	0.00
1097	KO					22		
1098	K K	SB/						
1099	BA	0.0481						
1100	LS	0.1	98.000			/5.000	0.1	
1101	ÛK	25	.02	.1	25.00			
1102	ÛK	6.0	.02	. 4	75.00			
1103	RD	600	.004	.02	.005	TRAP	2	25
1104	RD	1000	.004	.015		CIRC	1.5	
1105	KO					22		
1106	ΚK	SB5						
1107	ВA	0.0480						
1108	LS	0.1	98.000			76.000	0.1	
1109	UK	25	.02	.1	25.00			
1110	UK	60	.02	. 4	75.00			
1111	RD	600	.004	.02	.005	TRAP	2	25
1112	RD	1300	.004	.015		CIRC	2	
1113	KO					22		

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1114	KK	HC5									
1115	HC	2									
1116	ко					22					
1117	KK	CV4									
1118	RD	1472.34	0.00500	0.015		CIRC	2.50	0.00			
1119	KO					22					
1120	KK	SB4									
1121	BA	0.0194									
1122	LS	0.1	98.000			71.511	0.1				
1123	UK	25	.02	.1	15.03						
1124	UK	60	.02	. 4	84.97						
1125	RD	650	.004	.02	.0054	TRAP	2	25			
1126	RD	820	.004	.015		CIRC	3				
1127	KO					22					
1128	ΚK	HC2									
1129	HC	2									
1130	KO					22					
1131	кк	CV3									
1132	RD	531 325	0 00500	0 015		CIRC	3 0 0	0 0 0			
1133	ко	001.020	0.00000	0.010		22	0.00	0.00			
1100	110										
1134	ΚK	HC3									
1135	HC	2									
1136	KO					22					
1137	КК	DB1									
1138	RS	551	FLOW								
1139	SV	0	. 2.5	. 5	1	1.5	2	2.5	3	3.5	4
1140	SE	0	.25	. 5	1	1.5	2	2.5	3	3.5	4
1141	SO	0	2	4	6	8	9	10	11	12	12
1142	KO					22					
1143	ΚK	CV7									
1144	RD	418.687	0.02000	0.015		CIRC	2.00	0.00			
1145	KO					22					
1146	KK	SB50									
1147	BA	0.0252									
1148	LS	0.1	98.000			81.917	0.1				
1149	UK	25	.02	.1	16.54						
1150	UK	60	.02	. 4	83.46						
1151	RD	400	.01	.02		TRAP	2	25			
1152	KO					22					
1153	KK	DB9									
1154	RS	~	F.TOM	4	1 -	0	0 F				
1156	SV	0	0.5	1	1.5	2	2.5				
1157	SE	0	0.5	1	1.5	2	2.5				
1150	SQ	0	0.25	0.5	1	2	ΤU				
7 T 2 8	KO					22					

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1159	КК	CV31									
1160	RD	1146 65	0 01000	0 040		TRAP	4 0 0	2 0 0			
1161	KO	1110.00	0.01000	0.010		2.2	1.00	2.00			
1101	KO					22					
44.50											
1162	KK	SB51									
1163	BA	0.0473									
1164	LS	0.1	98.000			83.844	0.1				
1165	UK	2 5	.02	.1	0.10						
1166	UK	100	.02	. 4	99.90						
1167	RD	1000	.02	.04		TRAP	2	2			
1168	KO					22					
1169	КK	HC16									
1170	HC	3									
1171	КO					2.2					
11/1	110					22					
1170	14.14	0112.2									
1172	N.N.	250 050	0 01000	0 0 1 0			1 0 0	0 0 0			
11/3	RD	350.969	0.01000	0.040		TRAP	4.00	2.00			
1174	KO					22					
1175	ΚK	CV110									
1176	RD	1657.08	0.01000	0.040		TRAP	4.00	2.00			
1177	KO					22					
1178	ΚK	SB114									
1179	BA	0.0493									
1180	LS	0.1	98.000			77.000	0.1				
1181	UK	25	.02	. 1	25.00						
1182	IIK	60	0.2	4	75 00						
1183	PD	1000	.02	015	,0.00	CIRC	1.9				
1101	KD	1000	.02	.015		22	10				
1104	KO					22					
1105		avr1.1.5									
1185	KK	CVII5									
1186	RD	567.047	0.01000	0.014		CIRC	2.00	0.00			
1187	KO					22					
1188	KK	DB14									
1189	RS		FLOW								
1190	SV	0	.17	.33	.5	.66	.83	1	1.17	1.5	2
1191	SE	0	.33	.66	1	1.33	1.66	2	2.33	2.66	3
1192	SQ	0	2.3	4.6	6.9	9.2	11.5	15	20	28	60
1193	KO					22					
1194	КK	CV116									
1195	RD	485.929	0.00500	0.014		CIRC	1.50	0.00			
1196	KO					22					
2220	10										
1197	КК	SB100									
1100	D N	0 0360									
1100	BA	0.0300	00 000			77 000	0 1				
1200	LS	0.1	90.000	4	05 00	//.000	0.1				
1200	UK	25	0.02	.1	25.00						
1201	UK	60	.02	. 4	75.00						
1202	RD	1100	.02	.02		TRAP	2	25			
1203	KO					22					

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LINE	ID	1	2.		4.	5.	6 .	7.	8.	9.	10
1204	КК	USB1001	DETENTION	BASIN F	ROM REGU	LATED AF	REAS				
1205	КM	ELEVA	TION CURV	E IS VOL	UME IN A	C-FT OF	THEORETI	CAL DETE	NTION BA	SIN	
1206	RS		FLOW	0							
1207	SV	0 0000	0 0324	0 0655	0 0979	0 1404	0 1836	0 2261	0 2621	0 2945	0 327
1209	C F	0.0000	0.0324	0.0655	0.0979	0 1404	0.1836	0.2261	0.2621	0.2945	0.327
1200	20	0.0000	1 8896	2 6501	3 2/03	3 7563	4 2172	1 609	1 8391	5 0699	13 827
1210	5Q	0.0000	1.0050	2.0501	5.2495	3.7505	9.21/2	4.005	4.0554	5.0055	13.02/
1210	KU					22					
1011	VV	11 C Q 2									
1211	KK UC	ncos									
1212	HC	3				2.2					
1213	KU					22					
1014		GTT 1 1 0									
1214	K K	CVII8									
1215	RD	1032.63	0.01000	0.040		TRAP	4.00	2.00			
1216	KO					22					
1217	KK	HC61									
1218	HC	2									
1219	KO					22					
1220	ΚK	CV111									
1221	RD	209.613	0.01000	0.040		TRAP	4.00	2.00			
1222	KO					22					
1223	ΚK	SB101									
1224	BA	0.0234									
1225	LS	0.1	98.000			86.000	0.1				
1226	UK	50	.02	.14	60.00						
1227	UK	30	.02	. 4	40.00						
1228	RD	1100	.005	.015		CIRC	1.5				
1229	KO					22					
1230	KK	USB101	DETENTION	BASIN F	ROM REGU	LATED AF	REAS				
1231	КM	ELEVA	TION CURV	E IS VOL	UME IN A	C-FT OF	THEORETI	CAL DETE	NTION BA	SIN	
1232	RS		FLOW	0							
1233	SV	0.0000	0.0506	0.1023	0.1529	0.2192	0.2867	0.3530	0.4092	0.4598	0.511
1234	S F.	0.0000	0.0506	0.1023	0.1529	0.2192	0.2867	0.3530	0.4092	0.4598	0.511
1235	so	0.0000	1.2291	1.7238	2.1135	2.4433	2.7431	2.998	3.1479	3.2978	8.994
1236	KO					2.2					
1237	КК	SB86									
1238	D V	0 0186									
1239	DA T C	0.0100	98 000			77 000	0 1				
1240	1111	0.1 2E	0.000	1	25 00	,,	0.1				
12/1	U K	20	.02	• 1	23.00						
1241	UK	1200	.02	.4	13.00	CIDO	0				
1242	KD KD	1300	.02	.015		CIRC	Z				
⊥∠43	КO					22					
1044					Dow						
1244	KK	USB861	DETENTION	BASIN F	ROM REGU	LATED AF	KEAS				
1245	KM	ELEVA	TION CURV	E IS VOL	UME IN A	C-FT OF	THEORETI	CAL DETE	NTION BA	SIN	
1246	RS		FLOW	0							
1247	SV	0.0000	0.0168	0.0339	0.0507	0.0727	0.0951	0.1170	0.1357	0.1525	0.169
1248	SE	0.0000	0.0168	0.0339	0.0507	0.0727	0.0951	0.1170	0.1357	0.1525	0.169
1249	SQ	0.0000	0.9781	1.3717	1.6818	1.9442	2.1828	2.3856	2.5048	2.6241	7.156

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LINE	ID	1	2.		4.	5.	6.	7.	8.	9.	10
1250	KO					22					
1251	ΚK	HC59									
1252	HC	3									
1253	KO					22					
1254	ΚK	CV112									
1255	RD	337.416	0.01000	0.015		TRAP	4.00	2.00			
1256	KO					22					
1257	ΚK	SB79									
1258	ΒA	0.0156									
1259	LS	0.1	98.000			77.000	0.1				
1260	UK	2 5	.02	. 1	25.00						
1261	UK	60	.02	. 4	75.00						
1262	RD	800	.015	.015		CIRC	1.5				
1263	KO					22					
1051											
1264	K K	USB/91	DETENTION	BASIN F	ROM REGU	JLATED AR	EAS				
1265	KM	ELEVA	FION CURV	E IS VOL	JUME IN A	AC-F.L.OF.	THEORETI	CAL DETE	NTION BA	SIN	
1266	RS		FLOW	0	0 0 4 0 0	0 0 6 0 7	0 0700	0 0 0 7 7	0 1100	0 1070	0 1 4 1
1267	SV	0.0000	0.0140	0.0283	0.0423	0.0607	0.0793	0.0977	0.1132	0.1272	0.141
1268	SE	0.0000	0.0140	0.0283	0.0423	0.0607	1 0 0 1 7	1 001	0.1132	0.1272	0.141
1269	SQ	0.0000	0.8163	1.1448	1.4036	1.6226	1.821/	1.991	2.0905	2.1901	5.9/3
1270	кO					22					
1271	КК	CV82									
1272	RD	268 907	0 01000	0 015		CIRC	1 50	0 0 0			
1273	KO	200.007	0.01000	0.010		22	1.00	0.00			
12,0	110										
1274	КК	SB83									
1275	BA	0.0453									
1276	LS	0.1	98.000			77.000	0.1				
1277	UK	2.5	.02	.1	25.00						
1278	UK	60	.02	. 4	75.00						
1279	RD	800	.015	.015		CIRC	1.5				
1280	KO					22					
1281	КK	USB831	DETENTION	BASIN F	ROM REGU	JLATED AR	REAS				
1282	КM	ELEVA	TION CURV	E IS VOL	UME IN A	AC-FT OF	THEORETI	CAL DETE	NTION BA	SIN	
1283	RS		FLOW	0							
1284	SV	0.0000	0.0407	0.0824	0.1231	0.1765	0.2308	0.2842	0.3294	0.3702	0.411
1285	SE	0.0000	0.0407	0.0824	0.1231	0.1765	0.2308	0.2842	0.3294	0.3702	0.411
1286	SQ	0.0000	2.3748	3.3305	4.0835	4.7206	5.2998	5.7922	6.0818	6.3714	17.37
1287	KO					22					
1288	ΚK	CV83									
1289	RD	270.979	0.01000	0.015		CIRC	2.00	0.00			
1290	KO					22					

LINE 1291 KK SB108 BA 0.0397 1292 1293 LS 0.1 98.000 77.000 0.1 .1 25.00 1294 UK 25 .02 1295 UK 60 .02 .4 75.00 1296 RD 500 .02 .015 CIRC 1.5 1297 KO 22 1298 KK USB108DETENTION BASIN FROM REGULATED AREAS 1299 KM ELEVATION CURVE IS VOLUME IN AC-FT OF THEORETICAL DETENTION BASIN 1300 FLOW 0 RS 1301 SV 0.0000 0.0357 0.0722 0.1079 0.1547 0.2023 0.2491 0.2888 0.3245 0.361 1302 SE 0.0000 0.0357 0.0722 0.1079 0.1547 0.2023 0.2491 0.2888 0.3245 0.361 1303 SQ 0.0000 2.0816 2.9193 3.5794 4.1379 4.6456 5.0772 5.3310 5.5849 15.23 1304 ко 22 1305 KK CV62 RD 225.850 0.00500 0.015 1306 CIRC 1.50 0.00 1307 KO 22 1308 KK SB85 1309 BA 0.0157 77.000 1310 LS 0.1 98.000 0.1 1311 UK 25 .02 .1 25.00 1312 UK 60 .02 .4 75.00 1313 RD 100 .01 .015 CIRC 2 1314 KO 22 1315 KK USB85DETENTION BASIN FROM REGULATED AREAS 1316 KM ELEVATION CURVE IS VOLUME IN AC-FT OF THEORETICAL DETENTION BASIN 1317 RS FLOW 0 SV 0.0000 0.0142 0.0287 0.0428 0.0614 0.0803 0.0989 0.1146 0.1288 0.143 1318 SE 0.0000 0.0142 0.0287 0.0428 0.0614 0.0803 0.0989 0.1146 0.1288 0.143 1319 1320 SQ 0.0000 0.8261 1.1586 1.4205 1.6422 1.8437 2.015 2.1157 2.2165 6.045 1321 KO 2.2 1322 ΚK SB87 1323 BA 0.0283 1324 LS 0.1 98.000 77.000 0.1 .1 25.00 1325 UK 25 .02 1326 UK 60 .02 .4 75.00 CIRC 1327 RD 400 .02 .015 1.5 1328 KO 22 KK USB87DETENTION BASIN FROM REGULATED AREAS 1329 1330 KM ELEVATION CURVE IS VOLUME IN AC-FT OF THEORETICAL DETENTION BASIN 1331 RS FLOW 0 1332 SV 0.0000 0.0254 0.0514 0.0769 0.1102 0.1441 0.1775 0.2057 0.2312 0.257 1333 SE 0.0000 0.0254 0.0514 0.0769 0.1102 0.1441 0.1775 0.2057 0.2312 0.257 1334 SQ 0.0000 1.4831 2.08 2.5502 2.9481 3.3099 3.6174 3.7982 3.9791 10.852 1335 ко 22

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1336 КК НС44	
1338 KO 22	
1339 KK CV60	
1340 RD 1005.68 0.01690 0.014 CIRC 1.50 0.00	
1341 KO 22	
1342 KK SB96	
1343 BA 0.1079	
1344 LS 0.1 98.000 77.000 0.1	
1345 UK 25 .02 .1 25.00	
1346 UK 60 .02 .4 75.00	
1347 RD 1100 .015 .015 .02 TRAP 1.5	
1348 RD 700 .02 .015 CIRC 2	
1349 KO 22	
1350 KK CV72	
1351 RD 828.408 0.01500 0.015 CIRC 2.50 2.00	
1352 КО 22	
1353 KK CV76	
1354 RD 729.378 0.00600 0.015 CIRC 3.00 0.00	
1355 KO 22	
1056	
1356 KK 5897	
1357 BA 0.0365	
1358 LS 0.1 98.000 //.000 0.1	
1359 UK 25 .02 .1 25.00	
1360 UK $60$ $.02$ $.4$ $/5.00$	
1361 KD 400 .01 .015 CIRC 1.5	
1362 KU 22	
1363 KK HERRORDETENTION BASIN FROM RECHLATED AREAS	
1364 KR DEPUTION CIDUE IS VOLUME IN ACCEPT OF THEORETICAL DETENTION DASIN	
1365 PS FLOW 0	
	2000 0 332
1367 SF 0.0000 0.0329 0.0665 0.0994 0.1425 0.1863 0.2294 0.2659 0.	2988 0 332
1368 SO 0 0000 1 917 2 6884 3 2963 3 8106 4 2781 4 6756 4 9093 5	1431 14 026
	1401 14.020
2007 10 22	
1370 КК \$В95	
1371 BA 0.0492	
1372 LS 0.1 98.000 86.000 0.1	
1372      LS      0.1      98.000      86.000      0.1        1373      UK      50      .02      .14      60.00      0.1	
1372      LS      0.1      98.000      86.000      0.1        1373      UK      50      .02      .14      60.00        1374      UK      30      .02      .4      40.00	
1372  LS  0.1  98.000  86.000  0.1    1373  UK  50  .02  .14  60.00    1374  UK  30  .02  .4  40.00    1375  RD  1500  .01  .015  CIRC  1.5	

1

HEC-1	INPUT
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LINE	ID.	1	2.	3.	4.	5.	6.	7.	8.	9.	10	
1377	КК	USB951	DETENTION	BASIN F	ROM REGU	LATED AR	EAS					
1378	KM	ELEVAT	FION CURV	E IS VOL	UME IN A	C-FT OF	THEORETI	CAL DETE	NTION BA	SIN		
1379	RS		FLOW	0								
1380	SV	0.0000	0.1063	0.2149	0.3211	0.4604	0.6021	0.7414	0.8595	0.9657	1.074	
1381	SE	0.0000	0.1063	0.2149	0.3211	0.4604	0.6021	0.7414	0.8595	0.9657	1.074	
1382	SQ	0.0000	2.5815	3.6204	4.4389	5.1315	5.7612	6.2964	6.6112	6.9260	18.88	
1383	KO					22						
1384	KK	HC54										
1385	HC	3										
1386	KO					22						
1387	KK	CV73										
1388	RD	1308.82	0.02000	0.015		CIRC	2.50	0.00				
1389	KO					22						
1390	KK	CV75										
1391	RD	648.054	0.00800	0.015		CIRC	3.00	0.00				
1392	KO					22						
1393	ΖZ											

### SCHEMATIC DIAGRAM OF STREAM NETWORK

INPUT

LINE	(V) ROUTING	(>) DIVERSION OR PUMP FLOW
NO.	(.) CONNECTOR	(<) RETURN OF DIVERTED OR PUMPED FLOW
6	SB69 V V	
19	CV34 V	
22	CV35	
25	. SB59	
32	НС24 V	
35	V CV36	
38	. SB56 	
46	нс25 V	
49	CV10 V	
52	cv11	
55	. SB66 . V	
63	. cv37	
66	· · ·	SB77

	•	•	
73		HC26	
		V	
	•	V	
76		CV9	
	•	•	
	•	•	
79	•	•	SB55
	•	•	•
	•	•	•
87	•	НС7	
	•	V	
0.0	•	V	
90	•	CVIZ	
	•	•	
03	•	•	CD57
95	•	•	3037
	•	•	•
100	нся	•	•
100	V		
	V		
103	CV13		
	V		
	V		
106	DB2		
	V		
	V		
112	CV16		
	•		
	•		
115	•	SB60	
	•	V	
100	•	V	
123	•	DB3	
	•	V TZ	
120	•	CV1 /	
127	•	C V T H	
	•	•	
132	•	•	SB58
	•	•	•
140		HC10	

		V				
		V				
143		CV15				
	•	•				
146	НС9					
	V					
	V					
149	CV19					
152		SB63				
	•	•				
157	•	•	SB28			
			•			
	•	•				
162				SB27		
				•		
	•	•				
167	•	•			SB26	
				•	•	
				•	•	
172				•		SB25
	•	•		•	•	•
	•	•		•	•	•
177	•	HC38				
	•	V				
	•	V				
180	•	CV42				
	•	V				
	•	V				
183	•	CV41				
	•	V				
	•	V				
186	•	CV38				
	•	V				
	•	V				
189	•	CV39				
	•	•				
	•	•				
192	•	•	SB36			
	•	•	•			
	•	•	•			

200	. H	C18		
	•	V		
	•	V		
203	. C	:V40		
		V		
		V		
206		DB5		
		•		
		•		
212	•	•	SB34	
	•	•	•	
	•	•	•	
219	•	•	•	SB33
	•	•	•	•
	•	•	•	•
227	•	•	HC13	• • • • •
	•	•	V	
	•	•	V	
230	•	•	CV21	
	•	•	•	
	•	•	•	22.05
233	•	•	•	SB35
	•	•	•	•
0.4.1	·	•	•	•
241	•	•	HC14	• • • • •
	•	•	V	
244	•	•	V C C V Z	
244	•	•	CVZZ	
	·	•	V	
247	·	•		
21/	•	•	V	
	•	•	V	
253	•	•	CV23	
200	•	•		
256	. н	IC27		
	•	V		
		V		
259	. C	V18		
	•	V		
		V		
262	. CV	100		

265	•	•	CB113		
200	•	·	JDIIJ		
	•	•	V TZ		
272	•	•	CTV1 0 4		
212	•	•	CV104		
	•	•	•		
0.7.5	•	•	•	~~ ~ ~ ~ ~	
275	•	•	•	SB30	
	•	•	•	•	
	•	•	•	•	
283	•	•	•	•	SB111
	•	•	•	•	•
	•	•	•	•	•
291	•	•	•	HC80	
				V	
	•		•	V	
294			•	CV102	
			•	•	
297					SB112
305				HC73	
				V	
				V	
308	•	•	•	CV103	
000	•	•	•	01200	
	•	•	•	•	
311	•	•	ЦС79	•	
JII	•	·	110/9	• • • • • • • • • •	
	•	•	V TZ		
214	•	•			
314	•	•	DBIO		
	•	•	•		
	•	•	•		
320	HC12	• • • • • • • • • • • • • •	••••		
	V				
	V				
323	CV101				
	•				
	•				
326	•	SB110			
		V			
		V			
333		USB110			

	•	V	
		V	
340		CV105	
343			SB118
			V
			V
350	•	•	USB118
000	•	•	ODDIIO
	•	•	•
357	НС71	•	•
557	V		• • • • • • • • • •
	V 7.7		
200	0 C 1 7 D		
360	CVZU		
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0.00	•		
363	•	SB/2	
	•	V	
	•	V	
371	•	USB72	
	•	•	
	•	•	
378	HC28		
	V		
	V		
381	CV95		
	•		
	•		
384	•	SB75	
	•	V	
	•	V	
392		CV88	
		V	
		V	
395		CV89	
398			SB45
			V
		-	V
405		-	DB6
		-	- 200
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411				SB29
	•	•	•	•
419	•	•	HC78	• • • • • • • • •
	•	•	V	
	•	•	V	
422	•	•	CV91	
	•	•	•	
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425	•	•	•	SB73
	•	•	•	•
400	•	•	•	•
433	•	HC63	•••••	••••
	•	V		
100	•	V		
436	•	CV90		
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420	•	•	00100	
439	•	•	SBI03	
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4 4 7	•		•	
44/	•	нс64	• • • • • • • • •	
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450	•	۷ 12مم		
430	•	DBIJ		
	•	V TZ		
156	•	CV50		
400	•	CV30		
	•	•		
459	•	•	SBOO	
100	•	•	V	
	•	•	V	
466	•	•	USB99	
100	•	•	000000	
	•	•	•	
473	нс67	• • • • • • • • • • • • • •		
	V			
	V			
476	CV52			
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	•			
479		SB93		
		V		

	•	V		
486	•	USB93		
		V		
		V		
493		CV93		
496			SB94	
100	•	•	V	
	•	•	V	
503	•	•	USB94	
000	•	•	00001	
	•	•	•	
510	•	НС65	•	
510	•	11000		
	·	V 7.7		
512	•	CVQA		
515	•	CV 94		
	•	•		
F1 C	•	•		
210	HCSI	• • • • • • • • • •		
	V			
E10	V			
519	CV/1			
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500	•	0.00		
522	•	2898		
	•	V		
500	•	V		
529	•	USB98		
	•	•		
	•	•	10	
536	•	•	SB49	
	•	•	V	
	•	•	V	
544	•	•	USB49	
	•	•	V	
	•	•	V	
551	•	•	CV24	
	•	•	•	
	•	•	•	
554	•	•	•	SB48
	•	•	•	V
	•	•	•	V
562		•	•	USB48

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569	•	. HC55			
	•	. V	•		
	•	. V	<del>,</del>		
572	•	. CV64			
575			SB117		
0,0	•		V		
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503	•	• •	V 1100117		
505	•	• •	05DII/		
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590	•	• •	•	SB88	
	•	• •	•	V	
	•		•	V	
597	•		•	USB88	
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604	•		HC23.		
			V		
			V		
607			CV114		
	•				
610				SB91	
				V	
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617	•	• •	•	TICE Q1	
017	•	• •	•	USDJI	
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60.4	•	• •	•	•	0.000
624	•	• •	•	•	5889
	•	• •	•	•	V
	•	• •	•	•	V
631	•	• •	•	•	USB89
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	•	• •	•	•	•
638	•	. HC45			
		. V	•		
	•	. V	<del>,</del>		
641	•	. CV65			
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644	•	•		SB107	
				V	
				V	
651				USB107	
				V	
				V	
658				CV97	
000	•	•	•	V	
	•	•	•	77	
661	•	•	•	CVQ8	
001	•	•	•	0,000	
	•	•	•	•	
CCA	•	•	•	•	
664	•	•	HC68		
	•	•	V		
	•	•	V		
667	•	•	CV99		
	•	•	•		
	•	•	•		
670		•	•	SB90	
	•	•	•	V	
				V	
677				USB90	
				V	
				V	
684			_	CV66	
	•	•	•		
687	•	•	НС46	•	
007	•	•	10-10		
	•	•	V 77		
C 0 0	•	•	V		
690	•	•	CV67		
	•	•	•		
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693	•	•	•	SB92	
	•	•	•	V	
	•	•	•	V	
700				USB92	
		•			
707					SB104
					V
					V
714					USB104
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721			HC47		
			V		
	•	•	7.7		
	•	•	V		
724	•	•	CV68		
		•	•		
707	•	•	•	CD105	
121	•	•	•	SBIUS	
	•	•	•	V	
				V	
734				USB105	
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741			HC48		
			V		
			77		
744	•	•	OT T C O		
/44	•	•	CV69		
			•		
747				SB106	
111	•	•	•	JULUU	
	•	•	•	V	
	•	•	•	V	
754				USB106	
	•	•	•	•	
	•	•	•	•	
/61	•	•	HC49	• • • • • • • • •	
			V		
			V		
764			CV70		
704	•	•	0070		
	•	•	•		
	•	•	•		
767		HC50			
		V			
	•	77			
	•	V			
770	•	CV78			
		•			
772	•	-	CD10		
115	•	•	5040		
	•	•	V		
	•		V		
781			DB7		
			V		
	•	•	v 5.7		
	•	•	V		
787	•	•	CV25		

790	-	•	-	SB39	
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700	•	•	•	•	CD / 1
190	•	•	•	•	3D41
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805	•	•	нсзі	•••••	• • • • • • • •
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	•	•	V		
808	•	•	CV26		
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811	•	•		SB37	
				V	
				V	
819				CV53	
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822	•	•	•	•	SB38
022	•	•	•	•	5050
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830	•	•	•	нсээ	• • • • • • • • •
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833	•	•	•	CV27	
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836	•	•	•	•	SB43
			•		
	•		•		
843			HC32		
			V		
			V		
846			CV28		
010	•	•	0120		
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010	•	•	•	CD//	
049	•	•	•	SD44	
	•	•	•	•	
0.5.7	•	•	•	•	
857	•	•	нсз6	• • • • • • • • •	
	•	•	V		
			V		

		CV29			860
	SB46	•	•		863
	•	•	•	•	
	•	•	•	•	
		HC33.	•	•	870
		V	•	•	
		V	•	•	070
		CV30	•	•	8/3
		•	•	•	
	CD12	•	•	•	076
	5D4Z	•	•	•	070
	•	•	•	•	
	•	нсз <i>4</i>	•	•	883
		V	•	•	005
		V	•	•	
		DB8	•	•	886
		V	•	•	000
		V	•	•	
		CV119			892
		•	•		
	SB76				895
SB47					903
V					
V					
USB47		•	•	•	911
•	•	•	•	•	
•	•	•	•	•	
		HC37.	•	•	918
		V	•	•	
		V	•	•	
		CV55	•	•	921
		•	•	•	
	0004	•	•	•	0.0.4
	5884	•	•	•	924
	V * 7	•	•	•	
	V TICBOA	•	•	•	0.31
	03004	•	•	•	JJT
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938			HC20			
			77			
	•	•	V 7.7			
	•	•	V			
941	•	•	CV / 9			
	•	•	V			
		•	V			
944			CV61			
	•	•	•			
0.47	•	•	•	000		
947	•	•	•	SB82		
	•	•	•	V		
		•		V		
954				USB82		
	•	•	•	•		
0.61	•	•	•	•		
961	•	•	HC82			
	•	•	V			
		•	V			
964			CV84			
	•	•	•			
0.67	•	•	•	0001		
967	•	•	•	SB81		
	•	•	•	V		
				V		
974				CV59		
	•	•	•	•		
077	•	•	•	•	0070	
977	•	•	•	•	SB/8	
	•	•	•	•	V	
		•			V	
985	•				CV86	
	-	-			-	
000	•	•	•	•	•	0.000
988	•	•	•	•	•	SB80
	•	•	•	•	•	•
		•			•	•
995	•			HC60		
				V		
	•	•	•	77		
000	•	•	•	V DD1E		
998	•	•	•	DRID		
	•	•	•	V		
	•			V		
1004				CV85		

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		•		
1007	•	•	HC43	
			V	
			V	
1010	•	•	CV59	
1010	•	•	0000	
	•	•	•	
	•	•	•	
1013	•	•	•	SB116
				•
1020			HC41	
		-	V	
	•	•	77	
1000	•	•		
1023	•	•	CV57	
	•	•	•	
	•	•	•	
1026	•	•	•	SB115
				V
				V
1033				USB115
		-	-	V
	•	•	•	V
1040	•	•	•	CV100
1040	•	•	•	CV109
	•	•	•	•
	•	•	•	•
1043	•	•	HC81	• • • • • • • •
		•	V	
	•	•	V	
1046			CV117	
		-	•	
1040	•	•	•	CDC
1049	•	•	•	JDU
	•	•	•	V
	•	•	•	V
1056	•	•	•	CV5
	•	•	•	V
		•	•	V
1059				CV6
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# **APPENDIX B**

MODEL DESCRIPTION

## **RIVERTON CITY**

## HAL HYDROLOGIC MODEL FOR ARCVIEW

**USER'S MANUAL** 

Prepared by:

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# **INTRODUCTION**

This document serves as a how-to manual for the HAL Hydrologic Model interface with ArcView. The HAL Hydrologic Model Interface is a customization of the ArcView environment. All of the features of ArcView GIS are available when using the model because it runs inside of ArcView GIS. This manual only explains features that are unique to the HAL Hydrologic Model Interface. All other issues would be for standard features in the ArcView GIS environment. Help issues not related to the HAL Hydrologic Model Interface can be found in the ArcView GIS on-line help or user's manual.

This manual is organized as following manner.

The <u>Table of Contents</u> contains all of the help topics discussed in the manual. It is anticipated that the user will look in the table of contents to find the topic of interest.

<u>Project Setup</u> is discussed first, which covers the topic of how to setup and organize your project and scenarios contained within your project.

<u>Overview of the Scenario View</u> describes the environment where all of the features of the HAL Wastewater Collection Model customized ArcView extension are performed from except the project setup and organization features.

The Setup the Scenario section describes the features used to set up and define the scenario.

The function of each wastewater collection system feature is then described in the following order: <u>Subbasins</u>, <u>Conveyances</u>, <u>Confluences</u>, and <u>Diversions</u>.

The section, <u>Layouts</u>, describes how to print maps and data from the model using the Layout feature in ArcView. This section is quoted from the on-line user manual in ArcView because the Layout feature is part of ArcView and not the model.

## PROJECT SETUP

In ArcView, you work within a project. A project is a collection of documents (tables, charts, layouts, etc), document user interfaces, and scripts. Only one project is open at a time. Every ArcView project has a Project Window that you use to manage the views, tables, charts, layouts, scripts, and other components in the project. The project window in ArcView is like the table of contents to your project. A project with the HAL Hydrologic Model Interface extension loaded has a Storm Drain Scenario document user interface icon added to the Project Window. When the Wastewater Collection Scenario icon is selected, the scenarios in the project are listed. The Project Window is where the scenarios are managed. The tasks in this section are performed from the Project Window.



## How to create a new scenario:

- 1. In the Project Window, select the Wastewater Collection icon.
- 2. Select New
- 3. To change the name of the new scenario select Project Rename from the Menu Bar or select the Control and R keys.

## How to open a scenario:

- 1. In the Project Window, select the Wastewater Collection icon.
- 2. Select the scenario you want to open.
- 3. Select Open or double click on the scenario name you want to open.

#### How to create a new scenario from an existing scenario:

- In the Project Window, select the Wastewater Collection icon.
- Select the existing scenario that you want to create a new scenario from.
- Select Copy .
- To change the name of the new scenario select Project Rename from the Menu Bar.

# **OVERVIEW OF THE SCENARIO VIEW**

A view is an interactive map that lets you display, explore, query, and analyze geographic data in ArcView. The remaining tasks in the manual are performed from the Scenario View. The Scenario View contains the following features:

- The **Menu Bar** is a list of pull-down menus.
- The **Button Bar** is a list of button task controls.
- The **Tool Bar** is a list of tools that are used to interact with the View.
- The current **Scenario View** open is labeled at the top of the View window.
- The **Table of Contents** lists all of the geographical features in the View.
- The **View** is where the geographical features of the model scenario are viewed.

The following is a map of a Scenario View indicating these features.



# **SETUP THE SCENARIO**

To setup the Scenario, select Scenario – Setup from the Menu Bar. The Edit Dictionary window will open. The edit dictionary contains the properties that define the current scenario. To edit a property, click on the property and edit the parameters of the property. When done editing, select the Done button.

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# **SUBBASINS**

A Subbasin is an area defining wastewater loading. The attributes of a Subbasin are: Subbasin identification number, loading flow, and infiltration flow

## How to create a new Subbasin:

- 1. Select the Subbasin theme in the Table of Contents.
- 2. Start editing the Subbasin theme by selecting Theme Start Editing from the Menu Bar.
- 3. Draw the new Subbasin using the Draw Line tool from the Tool Bar.
- 4. Select Theme Stop Editing from the Menu Bar when done creating Subbasins. Save edits if desired.

## How to modify the shape of an existing Subbasin:

- 1. Select the Subbasin theme in the Table of Contents.
- 2. Start editing the Subbasin theme by selecting Theme Start Editing from the Menu Bar.
- 3. Select the Vertex Edit tool from the Tool Bar to edit the shape of the existing Subbasin.
- 4. Select Theme Stop Editing from the Menu Bar when done modifying Subbasins. Save edits if desired.

## How to modify the attributes of an existing Subbasin:

- 1. Select the Subbasin theme in the Table of Contents.
- 2. Select the Edit Attributes tool ATT from the Tool Bar and select the Subbasin to be

edited to open the Properties window.

3. Make edits to the Subbasin attributes in Properties window and select OK.

# **CONVEYANCES**

A Conveyance is a pipe that conveys wastewater from one point to another. The attributes of a Conveyance are: Conveyance identification number, length, slope, roughness coefficient, depth to diameter ratio, shape, diameter, capacity.

# How to create a new Conveyance:

- 1. Select the Conveyance theme in the Table of Contents.
- 2. Start editing the Conveyance theme by selecting Theme Start Editing from the Menu Bar.
- 3. Draw the new Conveyance with the Draw Line Tool from the Tool Bar.
- 4. Select Theme Stop Editing when done creating Conveyances. Save edits if desired.

# How to modify the shape of an existing Confluence:

- 1. Select the Confluence theme in the Table of Contents.
- 2. Start editing the Confluence theme by selecting Theme Start Editing from the Menu Bar.
- 3. Select the Vertex Edit tool from the Tool Bar to select and edit the existing Conveyance.
- 4. Select Theme Stop Editing from the Menu Bar when done modifying Conveyances . Save edits if desired.

# How to modify the attributes of an existing Confluence:

- 1. Select the Conveyance theme in the Table of Contents.
- 2. Select the Edit Attributes tool AII from the Tool Bar from the Tool Bar and select the

Conveyance to be edited to open the Properties window.

3. Make edits to the Conveyance attributes in the Properties window and select OK.

# **CONFLUENCES**

A confluence is a point where the wastewater flow form more than one Subbasin or Conveyance combines into one Conveyance. The attributes of a Confluence are the Confluence identification number and the number of flows from Subbasins and Conveyances are combined.

# How to create a new Confluence:

- 1. Select the Confluence theme in the Table of Contents.
- 2. Start editing the Confluence theme by selecting Theme Start Editing from the Menu Bar.
- 3. Create the new Confluence with the Draw Point tool in the Tool Bar.
- 4. Select Theme Stop Editing from the Menu Bar when done creating Confluences. Save edits if desired.

# How to modify the location of an existing Confluence:

- 1. Select the Confluence theme in the Table of Contents.
- 2. Start editing the Confluence theme by selecting Theme Start Editing from the Menu Bar.
- 3. Select the Pointer tool from the Tool Bar to select and move the Confluence.
- 4. Select Theme Stop Editing from the Menu Bar when done modifying Confluences. Save edits if desired.

# How to modify the attributes of an existing Confluence:

- 1. Select the Subbasin theme in the Table of Contents.
- 2. Select the Edit Attributes tool ATT from the Tool Bar and select the Confluence to be edited to open the Properties window.
- 3. Make edits to the Confluence attributes in the Properties window and select OK.

# **DIVERSIONS**

A Diversion is the splitting of wastewater flow from one Conveyance to more than one Conveyances or Confluences. Attributes of a Diversion are: Diversion identification number, the Conveyance or Confluence identification number of the Conveyance or Confluence the flow is being diverted to, and the percentage of wastewater flow being diverted to each Conveyance or Confluence.

## How to create a new Diversion:

- 1. Select the Diversion theme in the Table of Contents.
- 2. Start editing the Diversion theme by selecting Theme Start Editing from the Menu Bar.
- 3. Create the new Diversion with the Draw Point tool in the Tool Bar.
- 4. Select Theme Stop Editing from the Menu Bar when done creating Diversions. Save edits if desired.

## How to modify the location of an existing Diversion:

- 1. Select the Diversion theme in the Table of Contents.
- 2. Start editing the Diversion theme by selecting Theme Start Editing from the Menu Bar.
- 3. Select the Pointer tool from the Tool Bar to select and move the Diversion.
- 4. Select Theme Stop Editing from the Menu Bar when done modifying Diversions. Save edits if desired.

## How to modify the attributes of an existing Diversion:

- 1. Select the Diversion theme in the Table of Contents.
- 2. Select the Edit Attributes tool ATT from the Tool Bar and select the Diversion to be edited to open the Properties window.
- 3. Make edits to the Diversion attributes in the Properties window and select OK.

# SCENE MENU AND BUTTON BAR

The Scene Menu and Button Bar provides easy access to the functions needed to use the model. The Scene Menu is located in the Menu Bar. The Scene Menu and Button Bar contains the following features:



## How to run the model:

- 1. Open the Tool Box with the F2 key or by selecting Scenario Show Tool Box.
- 2. Select Scene Write Input from the Menu Bar or select *from the Button Bar to write an input file to disk in preparation to run the HEC-1 model.*
- 3. Select Scene Run from the Menu Bar to run the HEC-1 Model.

- 4. When the model has finished successfully, select Scene Read Results from the Menu Bar to read the results of the model run into ArcView. The Select Hydrograph File(s) window will open.
- 5. In the Select Hydrograph File(s) window that has opened, select the hydrograph file (\*.hyd) from the model run you wish to read into ArcView.

# How to view the results of a model run:

- 1. Select Scene View Results from the Menu Bar.
- 2. In the Select Summary File window, select the summary file (\*.sum) from the model run you wish to view the results.
- 3. To change the size of the results text, zoom in or out, and repeat steps 1 and 2.

# How to display flow curve in chart format:

- 1. Select Scene Toggle Hydrograph View in the Menu Bar to open the Select Base Time Series File window.
- 2. Select the Time Series Data (\*.hg) file in the Select Base Time Series File window that contains the data for the flow curve you wish to display.
- 3. Select YES and pick another Time Series Data file if you would like to display more than one flow curve in the same chart. Select NO when you are finished selecting the data files.
- 4. If the program cannot find the Link Field, it will ask you to pick the Field that will be the link.
- 5. If the program cannot find the Value field and Time field, you will be asked to identify them.

## How to use the Edit Attribute tool to edit the attributes of a Hydrologic Feature:

- 1. Select the theme of the Hydrologic Feature (Subbasin, Confluence, Diversion, or Conveyance) in the Table of Contents.
- 2. Select All from the Tool Bar and select the Hydrologic feature to be edited to open the Properties window.
- 3. Make edits to the attributes of Hydrologic Feature in the Properties window and select OK.

# How to use the Edit Connectivity tool to edit the connectivity of Hydrologic Features:

- 1. Select  $\Re$  from the Tool Bar.
- 2. Select the theme of the Hydrologic Feature (Subbasin, Confluence, Diversion, or Conveyance) in the Table of Contents.
- 3. Select the Hydrologic Feature to be edited to open the Input New Order window.
- 4. In the Input New Order window, input the new order number and select OK.
- 5. To edit the connectivity order of a different type of feature, select the theme of the Hydrologic Feature in the Table of Contents before selecting the feature with the Edit Connectivity tool.

# How to compute the area, length, and perimeter of selected features of the active theme(s):

- 1. Using the Select Feature tool from the Tool Bar, select the feature(s) for which you would like to compute the area, length, and/or perimeter.
- 2. Select the theme(s) of the features in the Table of Contents. Hold down the Shift key to select more than one.
- 3. Select **A** from the Button Bar.

# How to calculate Subbasin GIS attributes:

1. Select from the Button Bar. Subbasin attributes will be automatically calculated for every Subbasin.

# How to input or view Subbasin Hydrologic attributes:

- 1. Select the Subbasin theme in the Table of Contents.
- 2. Select the Select Feature tool from the Tool Bar and click on the Subbasin of interest or skip this step to input hydrologic attributes of all the Subbasins.
- 3. Select for from the Button Bar. A series of windows will open to input or view Subbasin Hydraulic Attributes.

# How to calculate capacities for Conveyances:

- 1. Select the Conveyance theme in the Table of Contents.
- 2. Select the Select Feature tool from the Tool Bar and click on the Conveyance of interest or select none to calculate capacities of all the Conveyances.
- 3. Select from the Button Bar. The capacity of the Conveyance(s) will be computed.

# How to size a Conveyance based on peak flow:

- 1. Select the Conveyance theme in the Table of Contents.
- 2. Select the Select Feature tool from the Tool Bar and click on the Conveyance(s) in which you want the size of the pipe to be adjusted to accommodate the peak flow calculated by the model.
- 3. Select **\*** from the Button Bar. The size of the pipe is adjusted to accommodate the peak flow calculated by the model.

# How to label the connectivity of the Hydrologic Features:

1. Select **C** from the Button Bar.

## How to zoom to selected features of the active theme:

- 1. Select the feature(s) you would like to inspect using the Select Feature tool from the Tool Bar.
- 2. Select the theme of the feature(s) in the Table of Contents.
- 3. Select for from the Button Bar.

# **LAYOUTS**

This section describes how to print maps and data from the model using the Layout feature in ArcView. Because the Layout feature is part of ArcView this section is quoted from the on-line user manual in ArcView.

A layout is a map that lets you display views, charts, tables, imported graphics, and graphic primitives. The layout is used to prepare these graphics for output from ArcView. A layout defines what data will be used for output and how they will be displayed. A layout can be dynamic because it allows you to make specific graphics live. When a graphic is live, it reflects the current status of the data. For example, if the data in a view changes, the layout automatically reflects the change.

The same data can be displayed on a number of different layouts. Think of each layout as being a different way of presenting the data. If you are doing a marketing presentation you will probably want to present data differently than if you are doing cartographic production. With ArcView, a different layout of the data can be created for each application. Using Avenue you can extend the power of ArcView by creating custom functions, user interfaces and cartographic templates that will assist you in creating output.

# What a layout can contain

The Layout provides the standard graphics and operations one would expect in a typical 'drawing' package. These graphics are drawn using the Draw tools and include points, lines, polygons, rectangles, and circles. The Layout also contains objects specific to the ArcView environment, including frames containing ArcView views, charts, and tables, and ancillary objects such as legends and scale bars.

# **Printing layouts**

You can print a layout or export a layout to a number of formats to use with other software packages.

# WORKING WITH LAYOUTS IN THE MODEL

An ArcView project can contain any number of layouts.

## How to see which layouts are in a project:

Click on the Layouts icon on the Project Window. The layouts in the current project are shown in the list.

## How to create a new layout:

With the Layouts icon selected, click the New button at the top of the Project window. ArcView creates a new layout and its name will appear in the list of layouts in the project. ArcView names new layouts in numerical order: Layout1, Layout2, Layout3, etc. See Overview of creating a layout. You can also double-click the Layouts icon to create a new layout.

## How to open a layout:

Double-click the layout's name in the list of layouts in the Project window, or select the layout's name and click the Open button.

## How to close a layout:

From the File menu, choose Close, or click the close option on the layout's window (This option varies according to the GUI you are using).

#### How to rename a layout:

Click once on the layout in the list in the Project window and choose Rename from the Project menu. A layout's name is also a layout property you can edit.

## How to save the work you do with a layout:

In ArcView, you save the work you do with any project component by saving the project. To save your project, choose Save Project from the File menu or click the Save Project button . See Saving your work.

## How to copy a layout from one project to another:

If you want to copy a layout from another project into your current project, you should import the other project into your current one using Import on the Project menu. This will copy all the components of the other project into your current project. You can then delete the components that you don't require using Delete from the Project menu.

# **CREATING A LAYOUT**

You create a layout from the components in your project such as views, charts, and tables. You can also draw various graphics on the layout too.

## How to open or create a project:

If you have not yet opened a project, choose Open Project or New Project from the File menu to either open an existing project or create a new one.

# How to create a new layout in your project:

On the Project window select the Layouts icon and then press the New button. A new layout will appear in your project.

# How to define the layout page:

Before you begin adding things to the layout, you should define some of its characteristics like units, page size, orientation and margins.

# How to add a view:

To create a map for output containing geographic data you must first add a view to your layout. When you add the view you can choose to make it live linked. This causes any changes in the view to be reflected in the layout. If you decide not to live link your view, it will not change in the layout even if you make changes to the view.

## How to add a legend:

After adding a view you can add a legend to the layout. The legend will show the symbology for the themes that are displayed in the view.

## How to add a scale bar:

There are a number of different styles of scale bars supported by ArcView. After you select a view to associate the scale bar to, you can select the type of units, interval values and number of intervals that the scale bar will have.

## How to add a title:

When you are satisfied with the geographically based parts of your layout you can add a title to it.

# How to create graphics:

If you need to add any graphic (points, lines, circles, etc.) you can do so.

# How to add other graphics to the layout:

There are a number of additional "standard" graphics you can add to your layout. You can place both ArcView tables and charts on the layout if so desired in your output product. You can also choose from a provided list of north arrows, or import a file from a another graphics package into the layout.

## How to arrange the layout graphics as needed:

When all of the graphics you want are present in the layout you can use a number of different tools to arrange them as needed. Among the actions you can perform on layout graphics are the following: align, bring to front, group, etc.

# How to assign patterns, colors and fonts to the graphics:

By double-clicking any graphic in the layout you can change its properties. In the case of a view or legend, you will see a properties menu. For any graphic primitive you will see ArcView's Symbol Window.

## How to Print the layout:

When you are finally satisfied with your layout you can send it to a printer.

# **APPENDIX C**

ESTIMATED CONSTRUCTION COSTS

#### RIVERTON CITY STORM DRAINAGE MASTER PLAN PROJECT COST ESTIMATES

West of Bangerter Highway

PROJECT NUMBER	DESCRIPTION	ROAD COSTS INCLUDED	DESIGN FLOW	MASTER PLAN SIZE	QUANTITY	UNITS	UNIT COST	TOTAL
1)	Western Springs to 4000 W Land Scaping				3	acre	\$15,000	\$45,000
	SD Structures & Field Drains				3	acre	\$20,000	\$60,000
	Earth Work				3	acre	\$20,000	\$60,000
	Land				3	acre	\$45,000	\$135,000
	Install pipe - Retention Pond to 12600 S	NO	22cfs	24	4,500	ft	\$73	\$328,500
	Install pipe - 12600 S to Swensen Farms	NO	27cfs	30	2,350	ft	\$95	\$223,250
	Mobilization							\$34,338
	SUB TOTAL							\$721,088
	Contingency & Engineering (30%)							\$216,326 <b>\$937 000</b>
2)								<i><b>*</b>••••</i> ,••••
-	Install pipe - 4600 S to Rose Creek	NO	7cfs	21	1400	ft	\$66	\$92,400
	Mobilization							\$4,620
	SUB TOTAL							\$97,020
	Contingency & Engineering (30%)							\$29,106
3)	TOTAL (rounded to hearest 1,000)							\$126,000
<i>c</i> /	Install pipe - 13200 S to Detention	NO	135cfs	42	1.550	ft	\$135	\$209.250
	Mobilization				.,			\$10,463
	SUB TOTAL							\$219,713
	Contingency & Engineering (30%)							\$65,914
	TOTAL (rounded to nearest 1,000)							\$286,000
4)	8 ac-ft Detention Basin							
	4320W & 13160S							
	Land Scaping			8.5 ac-ft	3	acre	\$15,000	\$45,000
	SD Structures & Field Drains				3	acre	\$20,000	\$60,000
					3	acre	\$20,000	\$60,000
	Land	NO	00 efe	20	3	acre	\$45,000	\$135,000
	Install pipe - Detention to Rose Creek	NO	20CTS	30	2500	π	\$95	\$237,500
								\$20,075 \$564 375
	Contingency & Engineering (30%)							\$304,373
	TOTAL (rounded to nearest 1.000)							\$734.000
5)								, ,,,,,,
	Install pipe - 5100 W east in 13400 S	NO		30	1600	ft	\$95	\$152,000
	Mobilization							\$7,600
	SUB TOTAL							\$159,600
	Contingency & Engineering (30%)							\$47,880
	TOTAL (rounded to nearest 1,000)							\$207,000
6)		NO	50 efe	20	1 200	e e	¢or	¢100 500
	Install Pipe - 4800 W in 13600 S	NO	50CIS	30	1,300	Π 4	\$95 \$116	\$123,500
	Mobilization	NO	70015	30	1,200	п	\$110	\$139,200 \$12,125
								\$13,133 \$275,835
	Contingency & Engineering (30%)							\$82 751
	TOTAL (rounded to nearest 1,000)							\$359,000
7)								
-	Install Pipe - 13000 S in 4600 W	NO	23cfs	30	1,600	ft	\$95	\$152,000
	Mobilization							\$7,600
	SUB TOTAL							\$159,600
	Contingency & Engineering (30%)							\$47,880
8)	IVIAL (rounded to nearest 1,000)							<b>⊅∠</b> ∪7,000
0)	4000 W 13200 S	NO	7cfs	18	600	ft	\$61	\$36.600
	4600W 13200 S to Rose Creek	NO	15cfs	24	600	ft	\$73	\$43,800
	Mobilization				200		ţ, o	\$4.020
	SUB TOTAL	İ		1				\$84,420
	Contingency & Engineering (30%)		1					\$25,326
	TOTAL (rounded to nearest 1,000)							\$110,000

PROJECT NUMBER	DESCRIPTION	ROAD COSTS INCLUDED	DESIGN FLOW	MASTER PLAN SIZE	QUANTITY	UNITS	UNIT COST	TOTAL
9)	1.5 ac-ft Detention Basin							
	4000W & 12300S							
	Land Scaping				1	acre	\$15,000	\$15,000
	SD Structures & Field Drains				1	acre	\$20,000	\$20,000
	Land				1	acre	\$20,000	\$20,000 \$45,000
	Install nine	NO		27	600	ft	\$84	\$50,000
	Install pipe	NO		30	800	ft	\$95	\$76.000
	Mobilization						¢00	\$11.320
	SUB TOTAL							\$237,720
	Contingency & Engineering (30%)							\$71,316
	TOTAL (rounded to nearest 1,000)							\$309,000
10)	4000 W 13000 S							
	Install pipe - 13000S to 13300S in 3900 W	NO		42	1,800	ft	\$135	\$243,000
	Install pipe - 3300S to Rose Cr in 3900 W	NO		48	1,350	ft	\$158	\$213,300
	Mobilization							\$22,815
	SUB TOTAL							\$479,115
	Contingency & Engineering (30%)							\$143,735
44)	2000 W and 12650 S to 2600 W and Dago							<b>\$023,000</b>
11)	3900 W and 13650 S to 3600 W and Rose	NO		20	800	f4	¢OF	\$76,000
,		NO		30	2 700	ft	ቆዓጋ ፍ116	\$70,000
	Mobilization	NO		50	2,700	11	\$110	\$19,200
	SUB TOTAL							\$408 660
	Contingency & Engineering (30%)				-			\$122,598
	TOTAL (rounded to nearest 1,000)							\$531,000
12)								
,	Install pipe - 4600 W to 4800 W in 13200 S	NO	75cfs	36	1800	ft	\$116	\$208,800
	Mobilization							\$10,440
	SUB TOTAL							\$219,240
	Contingency & Engineering (30%)							\$65,772
	TOTAL (rounded to nearest 1,000)							\$285,000
13)								
	Install pipe - 11800 S to Midas Creek in 4000	NO	7cfs	21	1150	ft	\$66	\$75,900
								\$3,795
	Contingency & Engineering (30%)							\$73,095
	TOTAL (rounded to nearest 1 000)							\$104 000
14)	4800W&13500S 5 ac-ft Detention							<i><i><i></i></i></i>
14)	Land Scaping				3	acre	\$15,000	\$45,000
	SD Structures & Field Drains				3	acre	\$20.000	\$60.000
	Earth Work				3	acre	\$20,000	\$60,000
	Land				3	acre	\$45,000	\$135,000
	Mobilization							\$15,000
	SUB TOTAL							\$315,000
	Contingency & Engineering (30%)							\$94,500
	TOTAL (rounded to nearest 1,000)							\$410,000
15)	1 ac-ft Detention Basin							
	4100S & 11990S							
	Lanu Scaping				0.5	acre	\$15,000	\$7,500
	SU Structures & Field Drains				0.5	acre	\$20,000 \$20,000	\$10,000 \$10,000
					0.5	acre	⊅∠0,000 ¢⊿⊑ 000	310,000 \$22 500
	Install nine	NO		18	0.5 500	ft	φ40,000 ¢ρ1	φ22,000 \$30 500
	Install pipe	NO		24	500	ft	\$73	\$36,500
	Mobilization			<u>_</u>	500		ψ/ 3	\$5 850
	SUB TOTAL							\$122.850
	Contingency & Engineering (30%)							\$36,855
	TOTAL (rounded to nearest 1,000)							\$160,000

PROJECT NUMBER	DESCRIPTION	ROAD COSTS INCLUDED	DESIGN FLOW	MASTER PLAN SIZE	QUANTITY	UNITS	UNIT COST	TOTAL
16)	Wasteway at Midas Creek and							
	Provo Resevoir Canal Wasteway				1	acre	\$10,000	\$10,000
	Mobilization					4010	\$10,000	\$500
	SUB TOTAL							\$10,500
	Contingency & Engineering (30%)							\$3,150 <b>\$14,000</b>
17)	134000 S and 4500 W to Rose Creek							<b>*</b> , <b>e</b> e e
-	Install pipe	NO	10cfs	21	1200	ft	\$66	\$79,200
	Mobilization							\$3,960
	Contingency & Engineering (30%)							\$83,160 \$24,048
	TOTAL (rounded to nearest 1,000)							\$108,000
18)	4000 W and 12700 S to Bangerter							
	Install pipe	NO	10cfs	18	1000	ft	\$61	\$61,000
	Mobilization							\$3,050
	Contingency & Engineering (30%)							\$04,050 \$19,215
	TOTAL (rounded to nearest 1,000)							\$83,000
19)	4400 W to 3950 W in 13000 S							
	Install pipe	NO	7cfs	18	1,450	ft	\$61	\$88,450
	Install pipe	NO	34cfs	30	1,550	ft	\$95	\$147,250
								\$11,785 \$247 485
	Contingency & Engineering (30%)							\$74,246
	TOTAL (rounded to nearest 1,000)							\$322,000
20)	12800 S to 13000 S in 4400 W							
	Install pipe	NO	4cfs	18	1,000	ft	\$61	\$61,000
								\$3,050 \$64,050
	Contingency & Engineering (30%)							\$19,215
	TOTAL (rounded to nearest 1,000)							\$83,000
21)	4300 W and 12800 S to 4200 W and 13000 S					_		
	Install pipe	NO	9cfs	18	1300	ft	\$61	\$79,300
	SUB TOTAL							\$3,900 \$83,265
	Contingency & Engineering (30%)							\$24,980
	TOTAL (rounded to nearest 1,000)							\$108,000
22)	12700 S to 13000 S in 4100 W			10				
	Install pipe Mehilization	NO	5cts	18	1,600	tt	\$61	\$97,600
	SUB TOTAL							\$102.480
	Contingency & Engineering (30%)							\$30,744
	TOTAL (rounded to nearest 1,000)							\$133,000
23)	12800 S to 13000 S in 3950 W	NO	Octo	24	700	<del>н</del>	<b>*</b> ~~	¢40.000
	Install pipe Mobilization	NO	9CTS	21	700	π	\$66	\$46,200 \$2,310
	SUB TOTAL							\$48,510
	Contingency & Engineering (30%)							\$14,553
	TOTAL (rounded to nearest 1,000)							\$63,000
24)	12350 S to 12200 S in 4300 W	NO		26	4 000	#	<b>#</b> 440	¢146.000
	Install pipe Mobilization	NO		30	1,000	π	\$116	\$116,000 \$5,800
	SUB TOTAL							\$121,800
	Contingency & Engineering (30%)							\$36,540
	TOTAL (rounded to nearest 1,000)							\$158,000
25)	Wasteway at Rose Creek and							
	Wasteway				1		\$10.000	\$10 000
	Mobilization				'		φ10,000	\$500
	SUB TOTAL							\$10,500
	Contingency & Engineering (30%)							\$3,150
	IOTAL (rounded to nearest 1,000)							\$14,000

ACRE 1836.5 TOTAL \$6,474,000 TOTAL/ARCE \$3,525

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Diamet <sup>ı</sup> (in)	er Diameter (ft)	Adjusted Cost per foot	Outside Diameter (ft)	Pipe Material & Installation	Excavation	Bedding	Hauling	Backfill Material & Installation	Trench Box per Day	Average Daily Output	Trench Box Cost	Top Trench Width	Manhole Cost	Inlet Cost	Total Cost per Foot of Pipe	Adjusted Cost per foot
	15 1.25	50.00	1.46	19.20	6.33	4.04	8.19	2.62	160.00	190.00	0.84	5.36	3.99	10.50	56	50
	18 1.50	61.00	1.75	29.00	6.76	4.62	8.75	2.79	160.00	130.00	1.23	5.65	3.99	10.50	68	61
	21 1.75	66.00	2.04	33.00	7.19	5.21	9.31	2.97	160.00	115.00	1.39	5.94	3.99	10.50	74	66
	24 2.00	73.00	2.33	39.50	7.62	5.82	9.87	3.15	160.00	100.00	1.60	6.23	3.99	10.50	82	73
	27 2.25	84.00	2.63	49.50	8.05	6.45	10.43	3.32	160.00	94.00	1.71	6.53	3.99	10.50	94	84
	30 2.50	95.00	2.92	59.50	8.48	7.10	10.99	3.50	160.00	88.00	1.82	6.82	3.99	10.50	106	95
	33 2.75	105.00	3.21	68.75	8.92	7.76	11.54	3.68	160.00	88.00	1.82	7.11	3.99	10.50	117	105
	36 3.00	116.00	3.50	78.00	9.35	8.44	12.10	3.86	160.00	72.00	2.22	7.40	4.34	10.50	129	116
	42 3.50	135.00	4.08	96.50	10.21	9.86	13.22	4.21	160.00	72.00	2.22	7.98	4.34	10.50	151	135
	48 4.00	158.00	4.67	115.00	11.07	11.34	14.34	4.57	160.00	64.00	2.50	8.57	6.61	10.50	176	158
	54 4.50	186.00	5.25	142.50	11.94	12.89	15.45	4.92	160.00	56.00	2.86	9.15	6.61	10.50	208	186
-	60 5.00	216.00	5.83	170.00	12.80	14.51	16.57	5.28	160.00	48.00	3.33	9.73	8.20	10.50	241	216
-	66 5.50	246.00	6.42	198.50	13.66	16.19	17.69	5.63	160.00	44.00	3.64	10.32	8.20	10.50	274	246
	72 6.00	275.00	7.00	227.00	14.52	17.95	18.80	5.99	160.00	40.00	4.00	10.90	8.20	10.50	307	275
	78 6.50	341.00	7.58	296.00	15.39	19.78	19.92	6.34	160.00	36.00	4.44	11.48	8.20	10.50	381	341
	84 7.00	407.00	8.17	365.00	16.25	21.67	21.04	6.69	160.00	32.00	5.00	12.07	8.20	10.50	454	407

Reference:

2004 Means Guide

One side of street C&G is regraded. Assumptions: PVC and Class III RCP Pipe

10 v :1h trench side slope (use trench boxes)

10 ' average depth to top of pipe

0.33 ' thick asphalt road covering 0.75 ' thick untreated base course

0.896 Salt Lake City adjustment factor

500 ' Average distance between manholes

2 + Outside Diameter = Bottom trench width

0.5 ' bedding over pipe

1 ' bedding under pipe

1 Inlets per 100 ft of pipe

0.4 of curb & gutter is on radius

0.045 Inflation (used in updating Utility Relocation costs).

1.95 /CY Imported granular backfill (p. 55, minimal haul)

Costs:

CY Pipe bedding (p. 56, Sand, dead or bank)
CY Excavation (p. 54, 10-14 ft deep, 1 CY backhoe)
SC Y 4" Asphalt Pavement (p. 72, 2" Binder, 2" Wear, p. 58, 9" Bank Run GravelBase Course; p. 56, Hauling)
A /LF 3" Asphalt cutting (p. 38)

1993 /EA 4' Manhous Oren 30, to be set 2.5' diameter, p. 92; p. 92, 30'' Ring & Cover) 2171 /EA 5' Manhole (for pipes =< 2.5' and <= 3.5', p. 92', p. 92, 30'' Ring & Cover) 3305 /EA 6' Manhole (for pipes > 3.5' and <= 4.5', p. 92; p. 92, 30'' Ring & Cover) 4100 /EA Manholes (for pipes > 4.5') 1050 /EA Catch basins (p. 91) 9.55 /LF Curb & Gutter (Steel forms, 24'' wide, p. 99)

4.7 /CY Hauling (p. 53, 2-mi round trip, 12 CY truck)

1 /LF Trench box

# **APPENDIX D**

SITE DEVELOPMENT STORM DRAINAGE AND EROSION CONTROL PLAN SUBMITTAL REQUIREMENTS

#### SITE DEVELOPMENT STORM DRAINAGE AND EROSION CONTROL PLAN SUBMITTAL REQUIREMENTS

#### **REVIEW PROCESS**

All subdivisions, resubdivisions, Planned Unit Development or any other development or redevelopment done within the jurisdiction of these CRITERIA shall be required to submit drainage reports, plans, construction drawings, specifications and as-constructed information in conformance to the requirements of these CRITERIA. Drainage aspects of these submittals are provided below. It is fully anticipated that the drainage components identified below will be included within the full submittal provided by the developer.

<u>Subdivision Process</u> The general requirements for the subdivision of land in Riverton City, and conditions requiring subdivision, are set forth in the Riverton City Development Code. Readers are referred to the development code for standards and procedures for the review and approval of subdivision plats.

<u>Permit Process</u> Any structure, or other development or redevelopment, which requires a building permit under the Riverton City code may also require a City Storm Drainage Permit to be issued by the Riverton City Engineering Department. These permits will only be issued upon conformance to requirements contained in these and other applicable CRITERIA as evidenced by approval of the Final Drainage Report.

#### A summary of submittals which are required of the developer to be submitted for Planning Commission review and approval include:

- A. Conceptual Level Drainage Control Plan. This plan is to be submitted for review by the Riverton City Flood Control Director for conceptual level feasibility.
- B. Preliminary Plan. This plan is to be submitted for review and preliminary approval by Riverton City Planning Commission and City Commission.
- C. Final Drainage Plan. The final drainage plan will be submitted subsequent to preliminary approval and must receive approval from both the Planning Commission and City Council. It is requested that review meetings be held with the developer prior to the preparation of the final drainage plan, and again prior to the development of final construction details and documents to help avert potential problems with final design. These meetings would be held prior to formal submittal of the final plans to the City Planning Commission and City Council.

The requirements for each of these plans are found within the following sections:

- 6. Conceptual Level Drainage Control Plan
- 7. Preliminary Drainage Control Plans
- 8. Final Drainage Control Plans, Plat and Document
- 9. As-built Drawings and Certification

#### **CONCEPTUAL LEVEL DRAINAGE CONTROL PLAN**

At the conceptual level the following general project information shall be provided to Riverton City for review and approval prior to the development of a Preliminary Plan.

#### **General Location and Description of Project**

- 1. Township, range, section, 1/4 section, (subdivision, lot and block).
- 2. Major drainage ways and facilities.
- 3. Area in acres.
- 4. Proposed land use.

#### **Drainage Basins and Sub-basins**

1. References to major drainage way planning studies such as flood hazard delineation reports, major drainage way planning reports, and flood insurance rate maps.

#### **Drainage Design Criteria**

- 1. Proposed drainage concept and how it fits existing drainage patterns.
- 2. Discussions of drainage problems, including storm water quality, and potential solutions at specific design points.
- 3. Discussion of detention storage and outlet design.
- 4. Discussion of minor and major drainage system.

#### Identification of Potential Improvements to Public Drainage Systems

1. Identification of potential design concepts and impacts to local drainage systems.

#### PRELIMINARY DRAINAGE CONTROL PLANS

At the time of land zoning, rezoning, or proposal for development or redevelopment, a preliminary drainage report is required in advance of the final drainage report. Ten copies of the preliminary drainage report, prepared and signed by a Professional Engineer registered in the State of Utah, shall be submitted to the Planning Commission for review. Reports shall be cleanly and clearly reproduced and legible throughout. Blurred or unreadable portions of the report will be deemed unacceptable and will require resubmittal. Incomplete or absent information may require resubmittal of the report.

The purpose of a preliminary report is to define on a conceptual level the nature of the proposed development or project and to describe all existing conditions and propose facilities needed to conform to the requirements of these CRITERIA. Each preliminary drainage report shall provide the following report information and mapping. It is recommended that the Preliminary Plan prepared by the developer follow the general outline provided below to facilitate City review.

#### **REPORT CONTENT**

#### **General Location and Description**

- A. Location
  - 1. City, County, State Highway and local streets within and adjacent to the site, or the area to be served by the drainage improvements.
  - 2. Township, range, section, 1/4 section, (subdivision, lot and block).
  - 3. Major drainage ways and facilities.
  - 4. Names of surrounding developments.
  - 5. Name of receiving water(s).
- B. Description of Property
  - 1. Existing ground cover (type and vegetation).
  - 2. Area in acres.
  - 3. Existing major irrigation facilities such as ditches and canals.
  - 4. Proposed land use and ground cover.

#### **Drainage Basins and Sub-basins**

- A. Major Basin Description
  - 1. References to major drainage way planning studies such as flood hazard delineation reports, major drainage way planning reports, and flood insurance rate maps.
  - 2. Major basin drainage characteristics, and existing and planned land uses within the basin, as defined by the planning commission.
  - 3. Identification of all nearby irrigation facilities that will influence or be influenced by the local drainage.
- B. Sub-Basin Description
  - 1. Describe historic drainage patterns of the property.
  - 2. Describe offsite drainage flow patterns and impact on development under existing and fully developed basin conditions.

#### **Drainage Facility Design Criteria**

- A. General Concept. Discuss the following:
  - 1. Proposed drainage concept and how it fits existing drainage patterns.
  - 2. How offsite runoff will be considered and how expected impacts will be addressed.
  - 3. Anticipated and proposed drainage patterns.
  - 4. Storm water quantity and quality management concept and how it will be employed. The use of computer-based models for the evaluation of storm water quality and quantity will not be universally required of new developments, although their use is recommended. Under site specific conditions where it is believed by the City that impacts from the development may unacceptably impact downstream water quality or quantity however, their use may be required. The recommendation to use computer modeling during the evaluation process is made since it is likely that the review process will check the validity of the developers conclusions utilizing SEDIMOT or other appropriate computer technology.

- 5. Maintenance and maintenance access.
- 6. Describe the content of tables, charts, figures, plates, drawings and design calculations presented in the report.
- B. Specific Details (Optional Information)
  - 1. Discussions of drainage problems, including storm water quality, and solutions at specific design points.
  - 2. Discussion of detention storage and outlet design.
  - 3. Discussion of impacts of concentrating flow on downstream properties.

#### **Public Drainage Improvements**

If the project requires that drainage improvements be constructed that will be turned over and owned and maintained by Riverton City, the following must also be provided, obtained, or completed:

A. A preliminary plan and/or design of the public improvement.

#### References

A. Reference all criteria, master plans, and technical information used in support of concept.

## MAPPING

#### **Preliminary Report Mapping**

- A. The General Location Map shall show the following information and conform to the following standards.
  - 1) All drawings shall be 22" x 34" in size.
  - 2) Map shall provide sufficient detail to identify drainage flows entering and leaving the development and general drainage patterns.
  - 3) The general location map should be at a scale of 1'' = 500' to 1'' = 4000' and show the path of all Drainage from the upper end of any offsite basins to the defined major drainage ways.
  - 4) Identify all major facilities (i.e., irrigation ditches, existing detention facilities, storm water quality facilities, culverts, storm sewers) downstream of the property along the flow path to the nearest major drainage way.
  - 5) Basins, basin identification numbers, drainage divides, and topographic contours are to be included.
- B. Flood plain Mapping:
  - 1) A copy of any published flood plain maps (i.e., flood hazard area delineation, flood insurance rate maps)
  - 2) All major drainage ways shall have the defined flood plain shown on the report drawings.
  - 3) Flood hazards from either shallow overland flow, side channels, or concentrated flows.
  - 4) The location of the property in relation to the flood plain(s) and/or flood hazards.
- C. Drainage Plan Mapping:
  - 1) Prepare at a scale of 1'' = 20' to 1'' = 200' on a 22'' x 34'' size drawing sheet.

- 2) Existing topographic contours at 2-feet (or less) intervals, In mountainous areas, the maximum interval may be extended to 5 feet. Final plan approval 1 foot contour intervals shall be shown for areas of little relief. The contours shall extend a minimum of 100-feet beyond the property lines.
- 3) All existing drainage facilities within map limits including basin boundaries and subboundaries.
- 4) Conceptual major drainage facilities including proposed storm water quality BMPs, detention basins, storm sewers, swales, riprap, and outlet structures in the detail consistent with the proposed development plan.
- 5) Any offsite feature including drainage that influences the development.
- 6) Proposed drainage patterns and, if available, proposed contours.
- 7) Legend to define map symbols.
- 8) Project name, address, engineering firm and seal, and date the Title block in lower right corner.
- 9) North arrow, scale and available bench mark information and location for each benchmark.

## FINAL DRAINAGE CONTROL PLANS, PLAT, DOCUMENT & CONSTRUCTION SPECIFICATIONS

The final drainage report serves to define and expand the concepts shown in the preliminary report or is sufficient of itself to assure conformance to these CRITERIA. The final report may be submitted at any point during the permitting and platting process, but <u>must</u> be reviewed and approved prior to issuance of any permit.

Ten (10) copies of the report shall be submitted to the Planning Commission. Reports shall be typed and bound on 8-1/2" x 11" paper with pages numbered consecutively. Drawings, figures, tables, etc., shall be bound with the report or contained in an attached pocket. The report shall include a cover letter presenting the design for review prepared or supervised by a Professional Engineer licensed in the State of Utah. The report shall contain a certification that reads as follows:

"This report for the drainage design of (name of development) was prepared by me (or under my direct supervision) in accordance with the provisions of the Riverton City storm drainage design and technical criteria, and was designed to comply with the provisions thereof. I understand that Riverton City does not and will not assume liability for drainage facilities design."

Registered Professional Engineer	
State of Utah No.	
(Affix Seal)	

#### **REPORT CONTENT**

The report shall be in accordance with the following outline and contains the following applicable information:

#### **General Location and Description**

- A. Location
  - 1. Information as required for Preliminary Plans.
  - 2. Local streets within the adjacent to the subdivision.
  - 3. Easements within and adjacent to the site.
- B. Description of Property
  - 1. Information as required for Preliminary Plans.
  - 2. General project description.
  - 3. Area in acres.
  - 4. General soil conditions, topography, and slope.
  - 5. Irrigation facilities.

#### **Drainage Basins and Sub-basins**

- A. Major Basin Description
  - 1. Information as required for Preliminary Plans.
  - 2. Identification of all irrigation facilities within the basin that will influence or be influenced by proposed site drainage.
- B. Sub-Basin Description
  - 1. Information as required for Preliminary Plans.

#### Drainage Facility Design Criteria

The design criteria used in the development of the drainage plan should be clearly identified including a discussion related to the use or implementation of any optional provisions intended by the developer or any deviation from the CRITERIA. Any deviation from the CRITERIA must be fully justified in the final design report. Development criteria should consider and discuss the following:

- A. Previous Studies and Specific Site Constraints
  - 1. Previous drainage studies (i.e., project master plans) for the site that influence or are influenced by the drainage design and how implementation of the plan will affect drainage and storm water quality for the site.
  - 2. Potential impacts identified from adjacent drainage studies.
  - 3. Drainage impacts of site constraints such as streets, utilities, transit ways, existing structures, and development or site plans.
- B. Hydrologic Criteria
  - 1. Design storm rainfall and its return period(s).
  - 2. Runoff calculation method(s).

- 3. Detention discharge and storage calculation method(s).
- 4. Discussion and justification of other criteria or calculation methods used that are not presented in or referenced by the CRITERIA.
- C. Hydraulic Criteria
  - 1. Identify various capacity references.
  - 2. Discussion of other drainage facility design criteria used that are not presented in these CRITERIA.
- D. Storm water Quality Criteria
  - 1. BMPs to be used for storm water quality control.
  - 2. Identify, as appropriate, water-quality capture volume and drain time for extended-detention basins, retention ponds and constructed wetland basins.
  - 3. Identify, as appropriate, runoff volume and flow rates for design of water-quality swales, wetland channels, etc.
  - 4. Discussion of other drainage facility design criteria used that are not presented in these CRITERIA or other manuals referenced by Riverton City.
- E. Waivers from Criteria
  - 1. Identify provisions by section number for which a waiver is requested.
  - 2. Provide justification for each waiver requested.

## **Drainage Facility Design**

Discuss the following:

- A. Proposed concept and typical drainage patterns.
- B. Compliance with offsite runoff considerations.
- C. Anticipated and proposed drainage patterns.
- D. Proposed storm water quality management strategy.
- E. The content of tables, charts, figures, plates, or drawings presented in the report.
- F. Drainage problems encountered and solutions at specific design points.
- G. Detention storage and outlet design.
- H. Storm water quality BMPs to be used.
- I. Maintenance access and aspects of the design.
- J. Easements and tracts for drainage purposes, including the conditions and limitations for use.

#### **Public Drainage Improvements**

If the project requires that drainage improvements be constructed that will be turned over and owned and maintained by Riverton City, the following must also be provided, obtained, or completed:

- A. Two sets of plans (22" x 34") submitted for initial review.
- B. An application to design, plan, construct, re-construct or remodel a public improvement must be filed with the Planning Commission.
- C. A bond or letter of credit guaranteeing payment and performance must be executed prior to commencing with work on the project.

- D. Upon completion of the project, a set of reproducible as-constructed plans, certified by a licensed engineer, must be submitted before the bond or other guarantee is released.
- E. After approval of the initial review set, ten (10) sets of plans must be supplied which will be distributed by the City for review by all departments and utility companies. After comments are received and addressed four (4) final sets will be stamped as approved and returned to the design engineer for use by the contractor and owner.

The information required for the plans shall be in accordance with sound engineering principles, the technical provisions of any City manuals (where appropriate), these CRITERIA, and other applicable Riverton City ordinances, regulations, criteria or design guidelines. The plans may also be subject to review by outside agencies such as Salt Lake County, Federal Emergency Management Agency, U.S. Army Corps of Engineers, Environmental Protection Agency, Utah Water, or other agencies as required. The plans shall be signed and sealed by a Professional Engineer registered in the state of Utah.

#### Conclusions

The Proposed Drainage Facility Plan will be evaluated based upon the material and data submitted in accordance with these CRITERIA and other manuals referenced by Riverton City. The plan must evaluate the effectiveness of the drainage design in controlling damage from storm runoff, in removing pollutants from storm runoff, and its potential influence on downstream drainages.

#### References

Reference all criteria and technical information used.

#### Appendices

Appendices should include all backup and supporting materials including:

- A. Hydrologic Computations (Including computer model input and output listings.)
  - 1. Land use assumptions regarding adjacent properties.
  - 2. Initial and major storm runoff at specific design points.
  - 3. Historic and fully-developed runoff computations at specific design points.
  - 4. Hydrographs at critical design points.
  - 5. Time of concentration and runoff coefficients for each basin.
  - 6. Storm water quality BMP sizing calculations including runoff adjustments for minimizing directly-connected impervious areas.
- B. Hydraulic Computations(Including computer model input and output listings.)
  - 1. Culvert capacities.
  - 2. Storm sewer capacity, including energy grade line (EGL) and hydraulic grade line (HGL) elevations.
  - 3. Gutter capacity as compared to allowable capacity.
  - 4. Storm inlet capacity including inlet control rating at connection to storm sewer.

- 5. Open channel design.
- 6. Check and/or channel drop design.
- 7. Detention area/volume capacity and outlet capacity calculations for flood detention and water quality basins; depths of detention basins.
- 8. Wetland area and area/depth distribution for constructed wetland basins.
- 9. Infiltration rates and volumes for porous pavement or release rates where under drains or infiltration is not possible.
- 10. Flow rates, velocities, longitudinal slopes and cross-sections for wetland channels and water quality swales.
- 11. Downstream/outfall system capacity to the Major Drainage way System.

#### MAPPING

#### **Final Report Mapping**

A. General Location Map.

Shall include all items as identified for the Preliminary Plan.

B. Flood plain Mapping.

Shall include all items as identified for the Preliminary Plan.

C. Drainage Plan Mapping.

In addition to those items identified for the development of the Preliminary Plan, Drainage mapping shall include the following:

- 1. Property lines, existing easements, and easements proposed for dedication, with purposes noted.
- 2. Streets, indicating ROW width, flow line width, curb or roadside swale type, sidewalk, and approximate slopes.
- 3. Existing drainage facilities and structures, including irrigation ditches, roadside ditches, cross pans, drainage ways, gutter flow directions, and culverts. Also, show pertinent information such as material, size, shape, slope and locations.
- 4. Proposed type of street flow (i.e., vertical or combination curb and gutter), roadside ditch or swale, gutter, slope and flow directions, and cross pans.
- 5. Proposed storm sewers and open drainage ways, including inlets, manholes, culverts, and other appurtenances, including riprap or other erosion protection.
- 6. Proposed structural water-quality BMPs, their location, sizing, and design information.
- 7. Proposed outfall point for runoff from the developed area and, if required, facilities to convey flows to the final outfall point without damage to downstream properties.
- 8. Routing and accumulation of flows at various critical points for the initial and water-quality storm runoff events, and major storm runoff events.
- 9. Volumes and release rates for detention storage and water-quality capture volume for facilities and information on outlet works.

- 10. Location and water surface profiles or elevations of all previously defined flood plains affecting the property. If flood plains have not been previously published, they shall be defined and shown on the drainage plan.
- 11. Location, and measured or estimated elevations of all existing and proposed utilities affected by or affecting the drainage design.
- 12. Routing of upstream offsite drainage flow through or around the development.
- 13. Location of any improvements included in the appropriate or accepted outfall system plan, major drainage plan, and/or storm drainage plan.
- 14. Definition of flow path leaving the development through the downstream properties ending at a major drainage way or receiving water.

#### **CONSTRUCTION PLANS**

For on-site drainage improvements, the final construction plans (22" x 34") shall be submitted after approval of the Final Drainage Report. Ten (10) sets of plans shall be submitted for approval. Upon approval, four sets, stamped and signed, will be returned to the design engineer for use by the contractor, owner and design engineer. However, before any construction work begins, appropriate bonds, letters-ofcredit, or other surety as required by these CRITERIA should be issued to Riverton City. The construction plans as a minimum and as appropriate will include:

- A. Plan and profile of proposed pipe installations, inlets and manholes with pertinent elevations, dimensions, type and horizontal control shown.
- B. Property and right-of-way lines, existing and proposed structures, fences and other land features.
- C. Plan and profile of existing and proposed channels, ditches swales, and on-site water-quality BMPs with construction details, cross-sections and erosion controls.
- D. Detention and water quality (if separate) facility grading, trickle channels (if any), outlet and inlet location, cross-sections or contours sufficient to verify volumes, etc.
- E. Details of inlet and outlet control devices and of all structural components being constructed.
- F. Maintenance access.
- G. General over lot grading and the erosion and sediment control plan prepared in accordance with applicable provisions of these CRITERIA and the MANUAL.
- H. Areas of modular block porous pavement, if any, and installation details.
- I. Landscaping and revegetation plans and details.
- J. Proposed finish floor elevations of structures.
- K. Relation of site to current and, if appropriate, modified flood plain boundaries.
- L. A statement agreeing to maintain and operate all privately-owned facilities (if any) in a working manner and/or in accordance with the requirements of the Utah Water Quality Control Division specified in the storm water discharge permit issued to Riverton City.
- M. Signature and seal of a professional engineer preparing these plans.

Approval by Riverton City does not constitute an approval or the issuance of permits by the State of Utah, which approval and/or permits shall be obtained prior to initiating any construction activities on the site.

## AS-BUILT DRAWINGS AND CERTIFICATION

Upon completion of construction, the professional engineer that prepared the design plans (or a professional engineer that assumes the responsibility for the inspection if the design engineer is no longer available) shall provide Riverton City with a signed and sealed Certification of Inspection verifying that all work was performed in accordance with the approved plans and in compliance with all applicable criteria of Riverton City and that any changes which occurred during construction are included in the as-built drawings. Special circumstances may require that as-built reproducible drawings of the drainage improvements also be provided. Certification of Inspection and as-built drawings (if required) will be required prior to the issuance of a final sewer connection permit or the issuance of a Certificate of Occupancy.